

DIGITAL WE DAYS

2023



DESIGN CONSIDERATIONS FOR
FLYBACK TRANSFORMER

WÜRTH ELEKTRONIK MORE THAN YOU EXPECT

TODAY'S SPEAKERS



PRESENTATION

Khaled Elshafey
Design Engineer



MODERATION

Silas Zorn
Marketing Department

INFORMATION ABOUT THE WEBINAR

You are muted during the webinar.

However, you can ask us questions using the chat function.

Duration of the presentation 30 Min
Q&A: 10 – 15 Min

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On our channel Würth Elektronik Group
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AGENDA

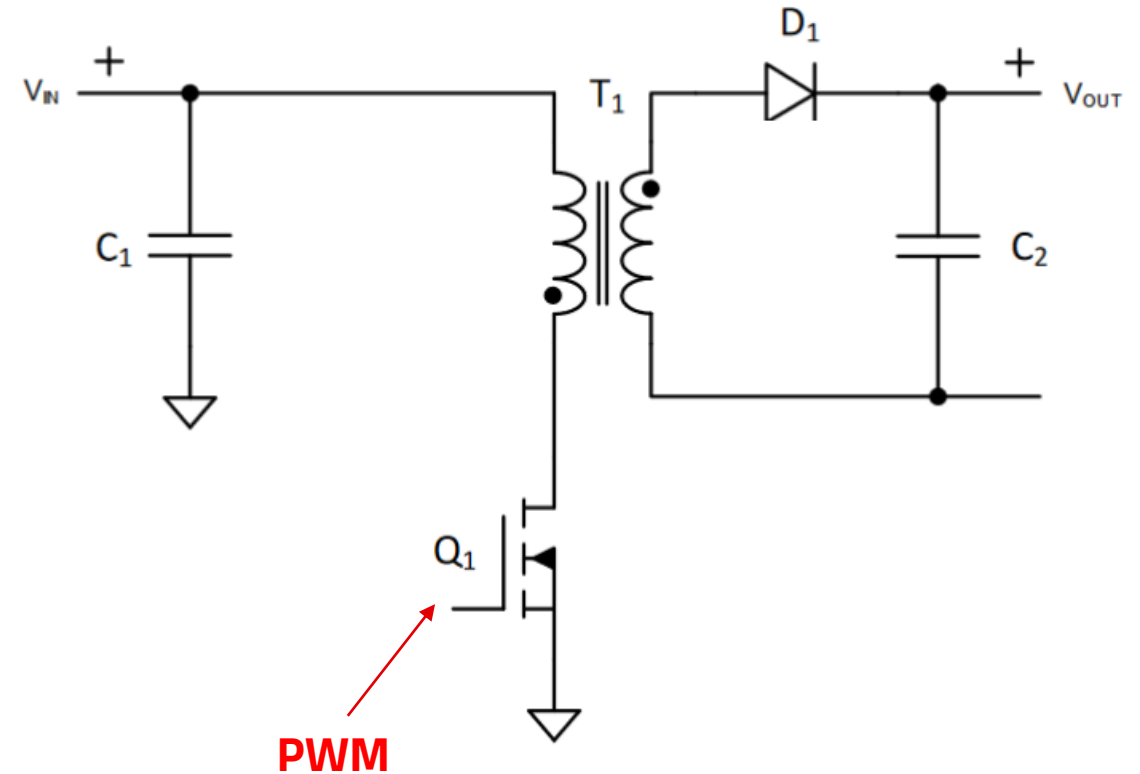
- Short overview -What is flyback topology
- Short overview - Mode of operation
- Flyback transformer – Design Requirements
- Methods to improve some of Flyback transformer characteristics
- Tips to improve EMI



SHORT OVERVIEW

What is Flyback Topology

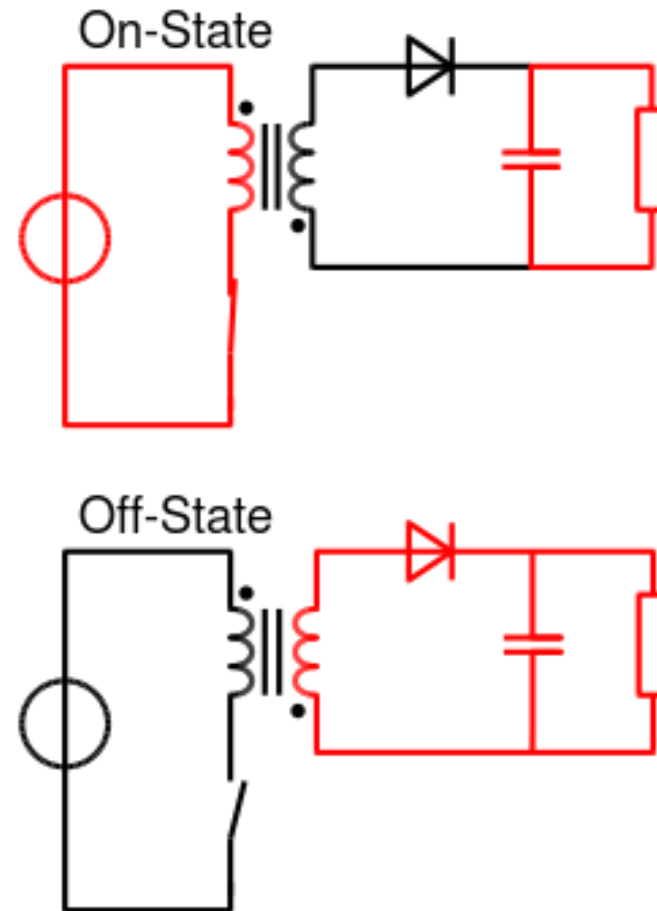
- It is one of modern SMPS topology uses PWM techniques
- It can provide isolation using transformer
- Controller is not complicated
- A few components needed to build the circuit
- Typically uses for power range < **100 watts**



SHORT OVERVIEW

What is Flyback Topology

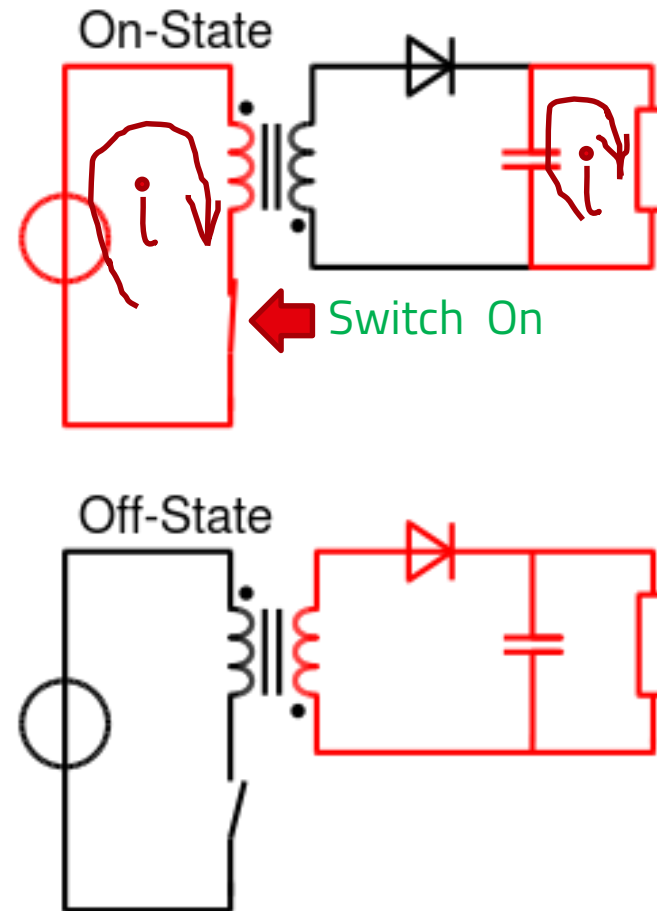
- How does it work?
 - Two states of operation:
 - On state
 - **Off state**



SHORT OVERVIEW

What is Flyback Topology

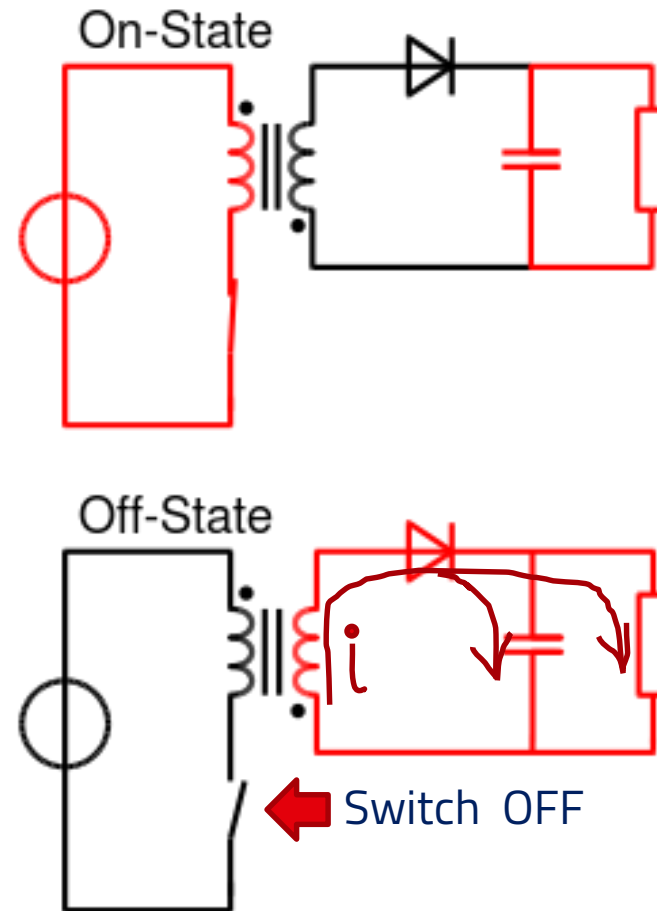
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SHORT OVERVIEW

What is Flyback Topology

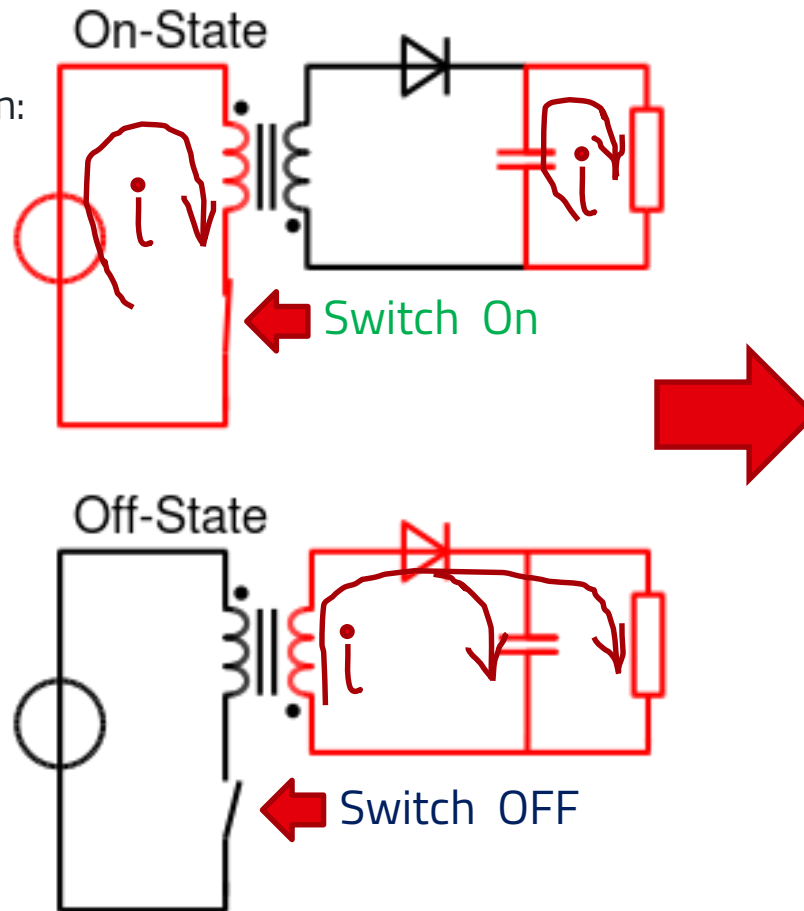
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SHORT OVERVIEW

What is Flyback Topology

- How does it work?
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Flyback transformer is **NOT** a real transformer

No transfer energy **instantaneously**

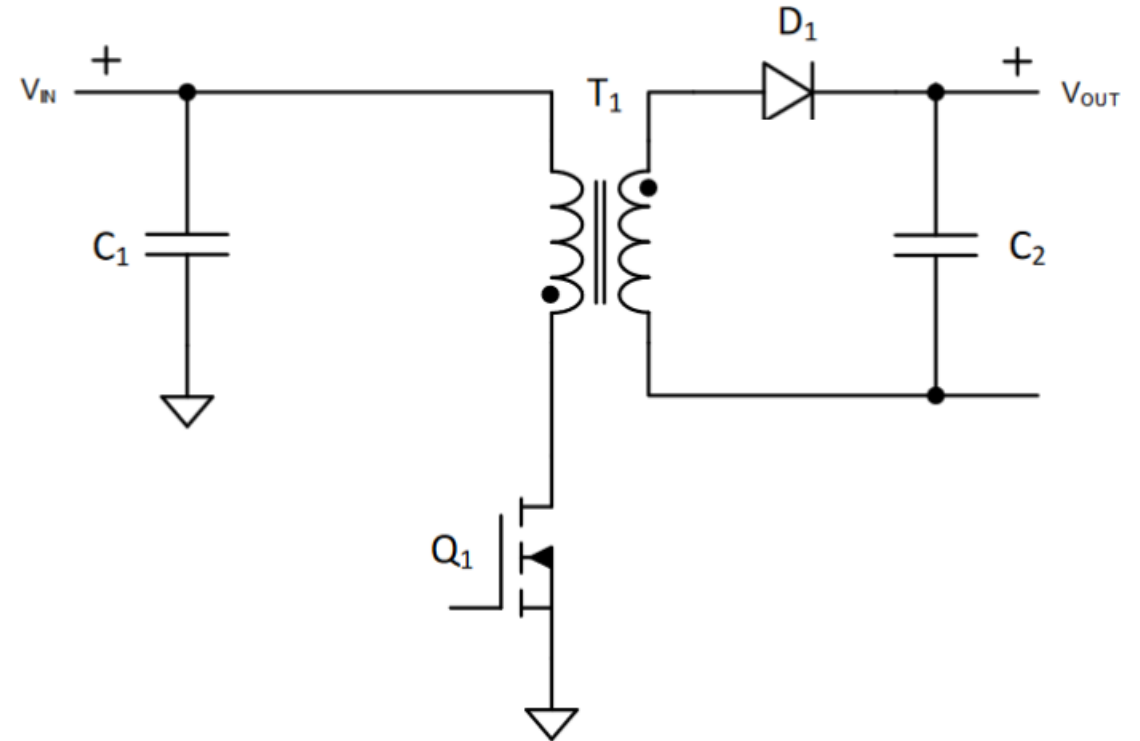
Acts as inductor **store** energy then release it

So sometimes called it a **Coupled Inductor**

SHORT OVERVIEW

What is Flyback Topology

- **Advantages:**
 - Controller is not complicated
 - A few components needed to build the circuit
- **Disadvantages:**
 - Generate high ripples -> EMI issues
 - Monitor leakage inductance -> to protect Mosfet
 - Not suitable for applications require high efficiency



SHORT OVERVIEW

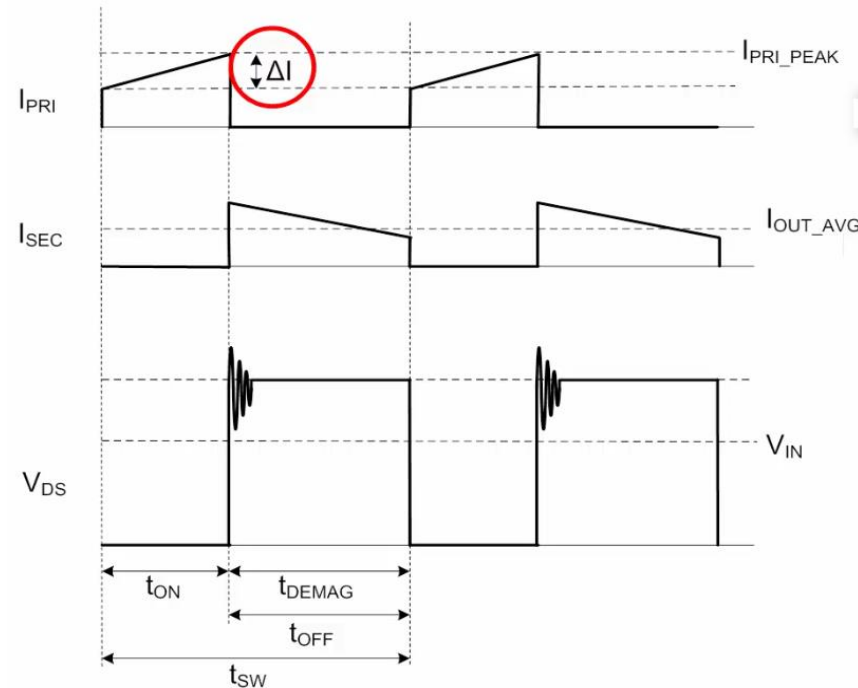
Mode of operation

- There are many text books and application notes talk and explain about Flyback operation mode
- Here is a summary about mode of operations:

SHORT OVERVIEW

Mode of operation

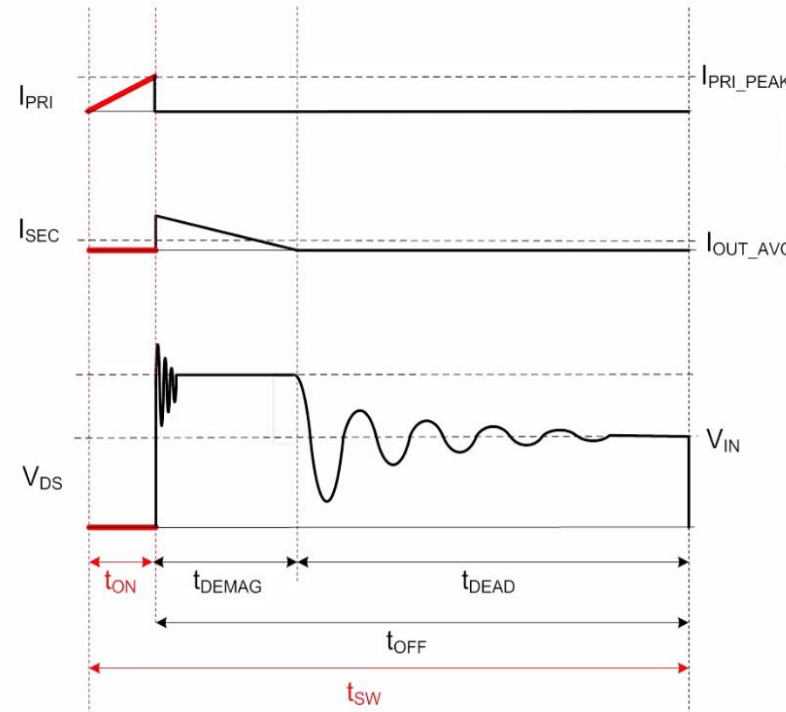
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SHORT OVERVIEW

Mode of operation

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 - **CCM**: Continuous Conduction Mode – Fixed frequency
 - **DCM**: Discontinuous Conduction Mode - Fixed frequency



SHORT OVERVIEW

Mode of operation

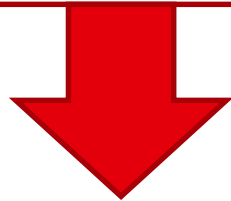
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 - **CCM**: Continuous **C**onduction **M**ode
 - **DCM**: Discontinuous **C**onduction **M**ode
 - Special cases from **DCM** with **variable switching frequency**:
 - Quasi-Resonant Mode or transition mode or Critical condition mode
 - Valley Switching

SHORT OVERVIEW

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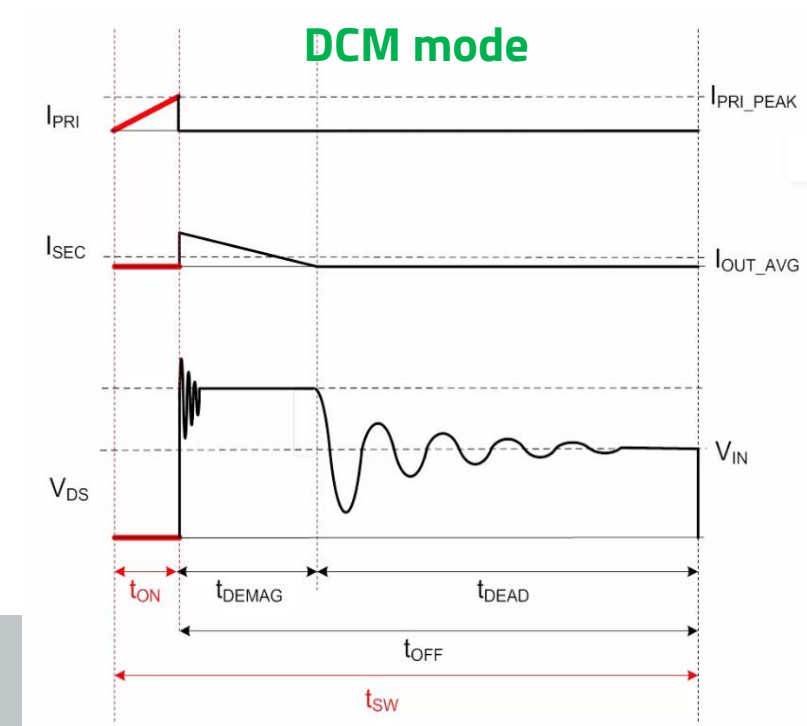
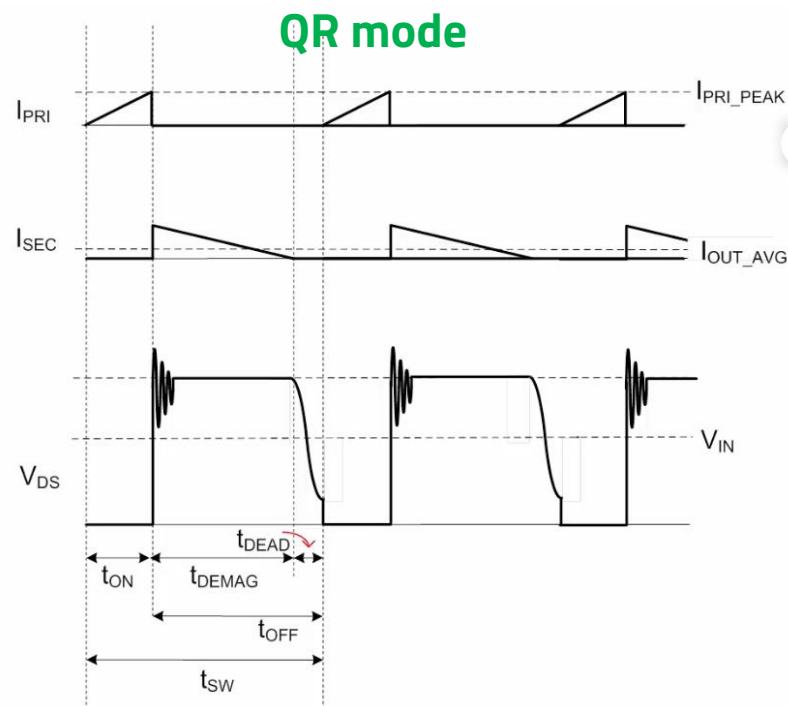


Common mode of operation for ICs have a **Primary Side Regulation** feature
– **No feedback loop needed (Optocoupler)**

SHORT OVERVIEW

Mode of operation

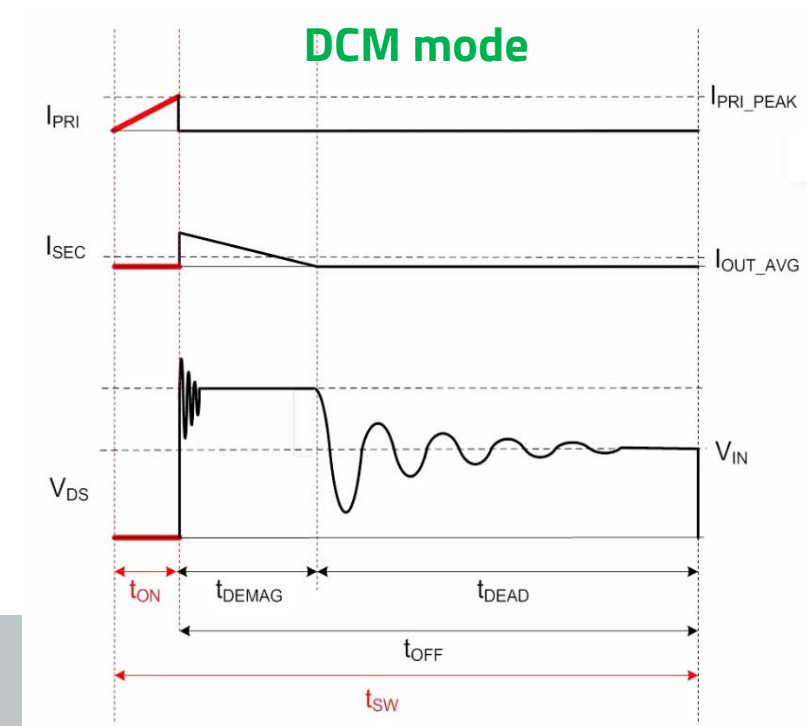
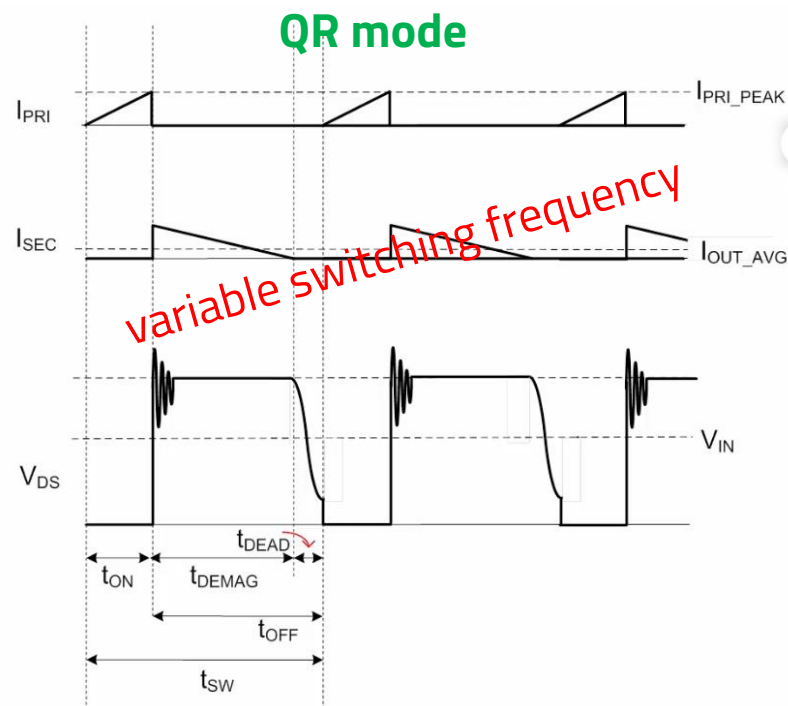
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FLYBACK TRANSFORMER

Design Requirements

- You notice that Flyback transformer store energy on core then release it, So

$$\text{Energy (store inside core)} = \frac{1}{2} \frac{B^2}{\mu_c} V_c \quad \text{unit J}$$

Where:

B: Flux density

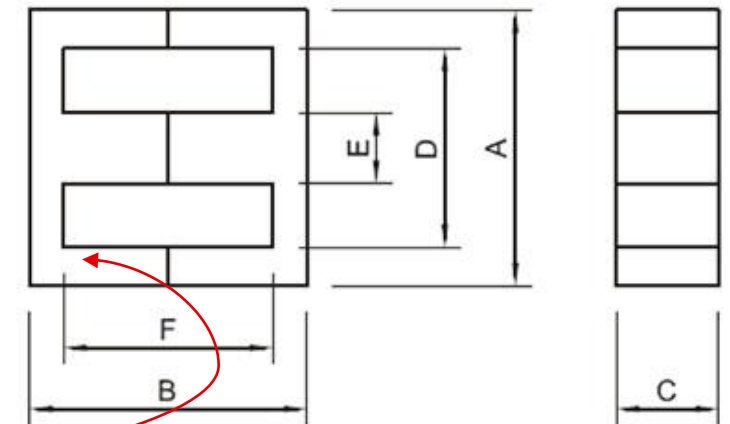
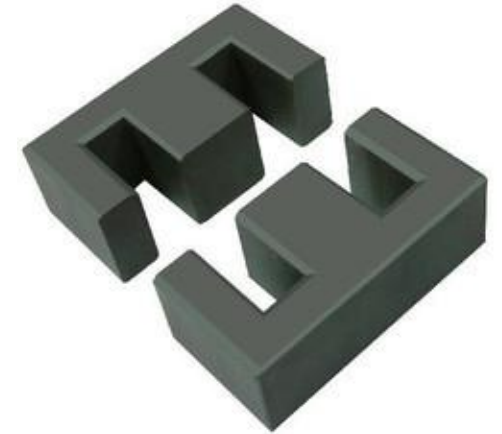
μ_c : Core permeability

V_c : Core volume

$$\text{Energy} \propto \frac{V_c}{\mu_c}$$

$$\uparrow \text{Energy} \propto \frac{\uparrow V_c}{\mu_c}$$

$$\uparrow \text{Energy} \propto \frac{V_c}{\downarrow \mu_c}$$



For un-gapped core, μ_c about 1500 to 6000

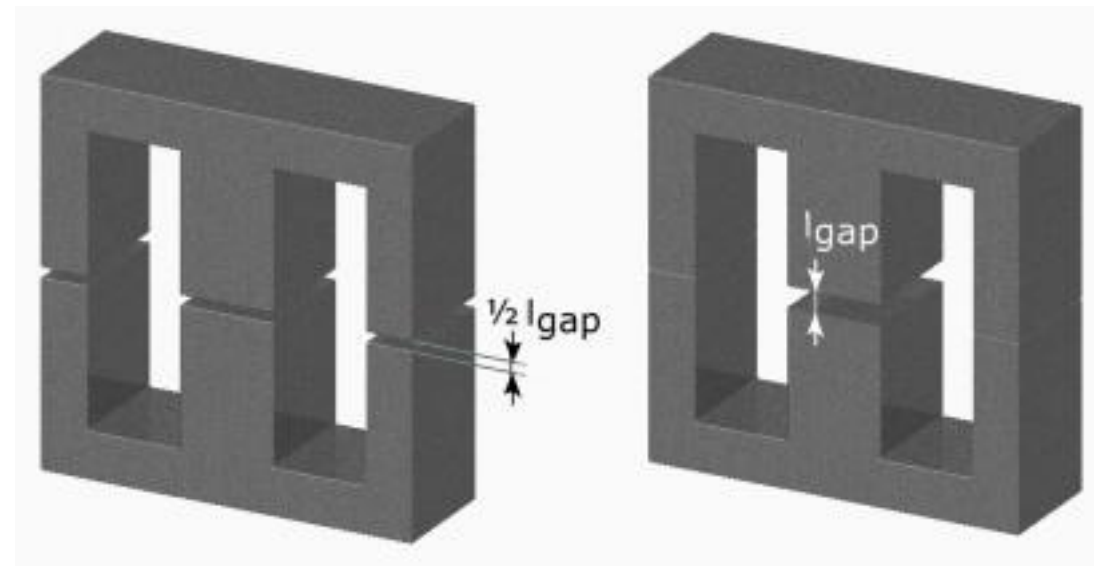
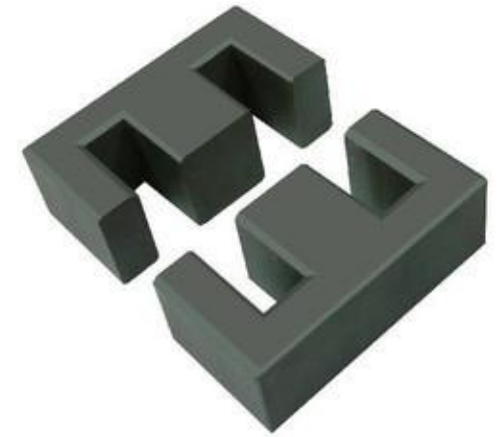
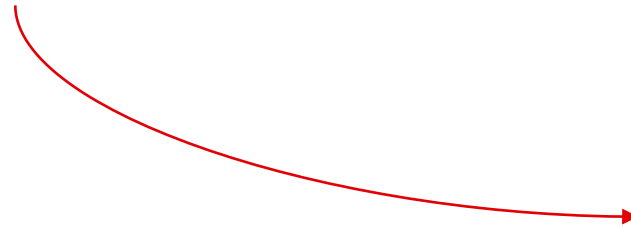
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$$\uparrow \text{Energy} \propto \frac{V_c}{\downarrow \mu_c}$$

Add an air gap to core to reduce the equivalent permeability



FLYBACK TRANSFORMER

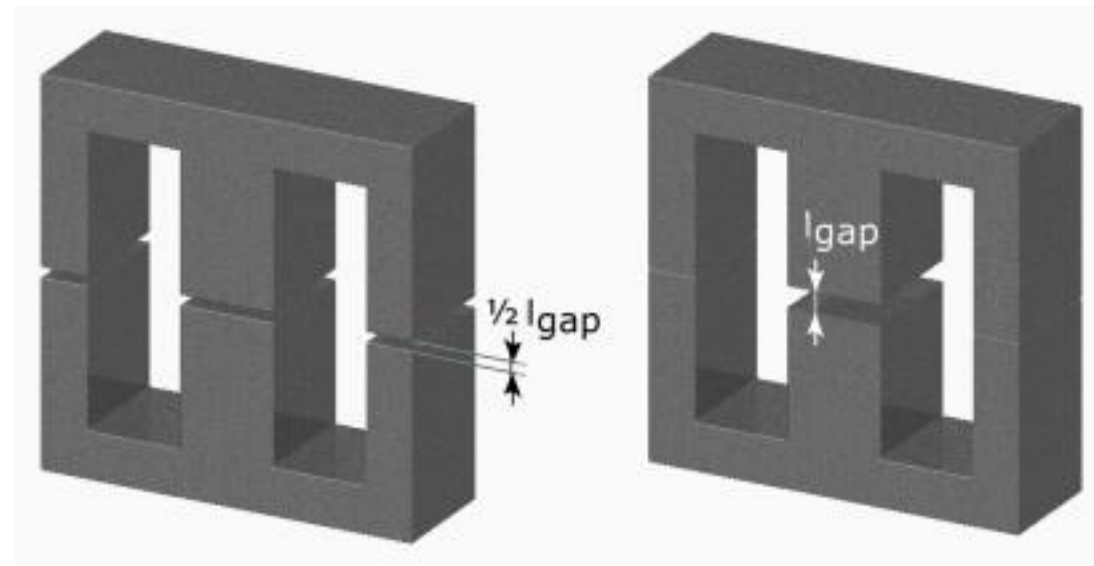
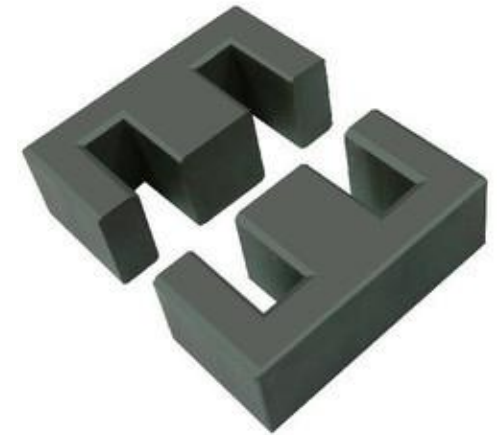
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$$\text{Energy (store in an inductor)} = \frac{1}{2} L_{ind} I^2$$

$$\text{Max. Energy (store in an inductor)} \approx \frac{1}{2} L_{ind} I_{sat}^2$$

$$I_{sat-prim} \gg I_{Pri} \text{ or required for design}$$



FLYBACK TRANSFORMER

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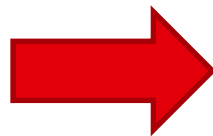
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⑥C ELECTRICAL SPECIFICATIONS @ 25°C unless otherwise noted:

PARAMETER		TEST CONDITIONS	VALUE
D.C. RESISTANCE	1-3	@20°C	3.15 ohms ±10%
D.C. RESISTANCE	5-4	@20°C	0.81 ohms ±10%
D.C. RESISTANCE	7-9	tie(6+7, 8+9), @20°C	0.021 ohms ±20%
INDUCTANCE	1-3	10kHz, 100mVAC, Ls	1.59mH ±10%
SATURATION CURRENT		20% rolloff from initial	480mA
LEAKAGE INDUCTANCE	1-3	tie(4+5, 6+7+8+9), 100kHz, 100mVAC, Ls	23uH typ., 34uH max.
⑥C DIELECTRIC	3-7	tie(3+4, 7+8), 4500VAC, 1 second	3600VAC, 1 minute
URNS RATIO		(3-1):(7-9), tie(6+7, 8+9)	15:1, ±1%
URNS RATIO		(3-1):(5-4)	8.571:1, ±1%

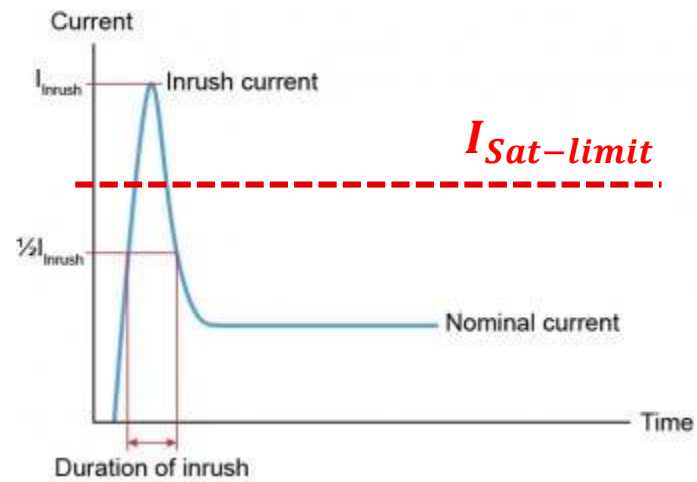
**Important requirement
for Flyback transformer**



FLYBACK TRANSFORMER

Design Requirements

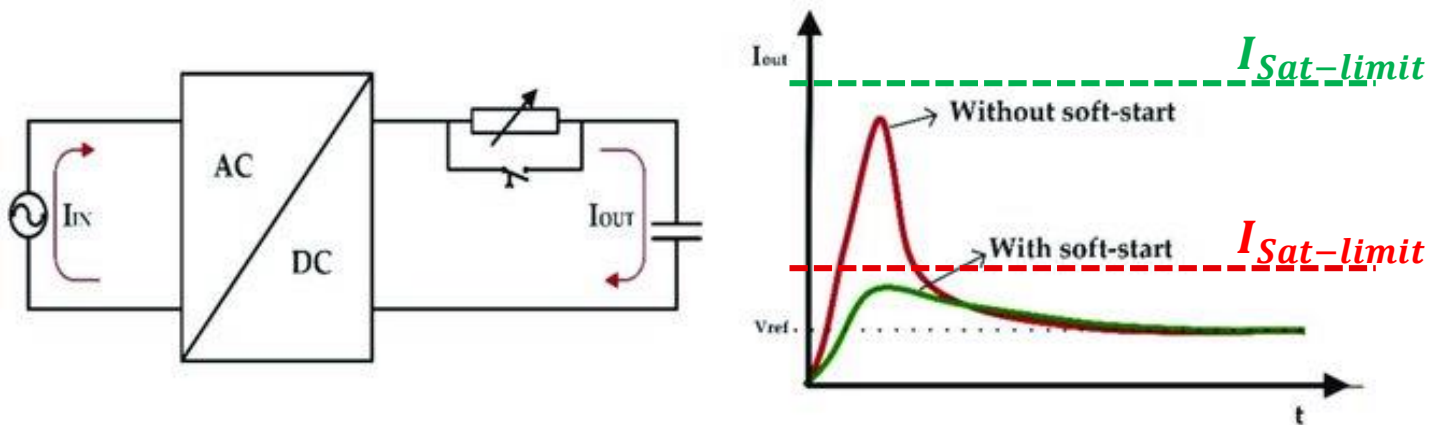
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- **Very important note:**
 - During the start up of the power supply, Inrush current can exceed saturation current:



FLYBACK TRANSFORMER

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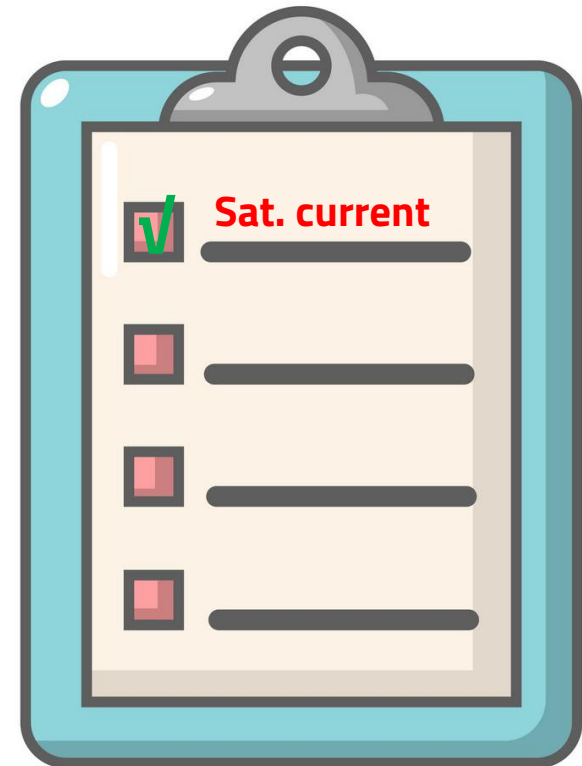
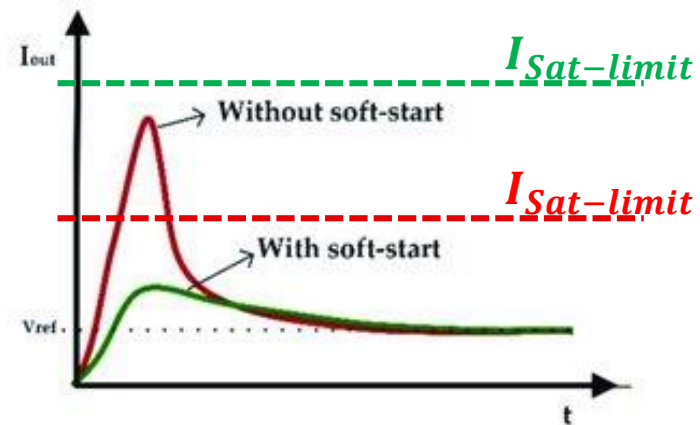
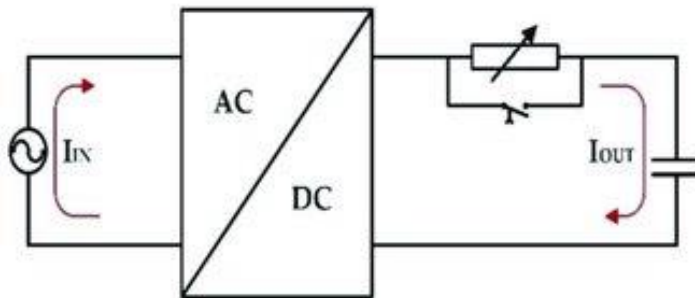
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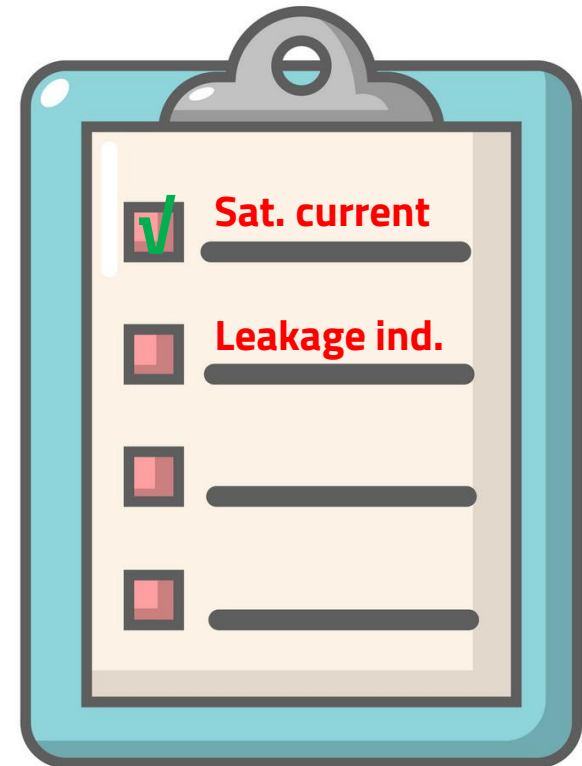
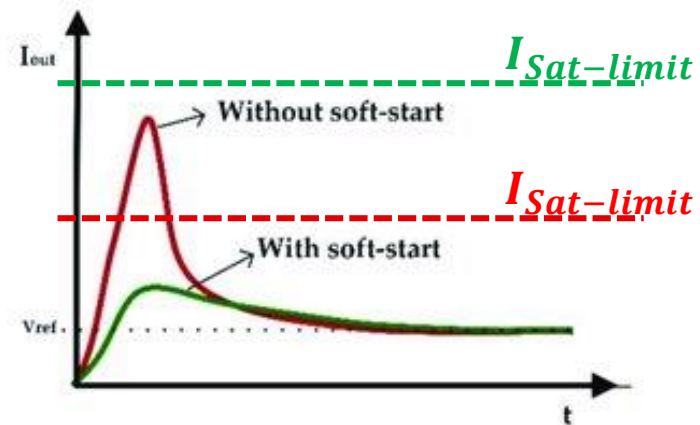
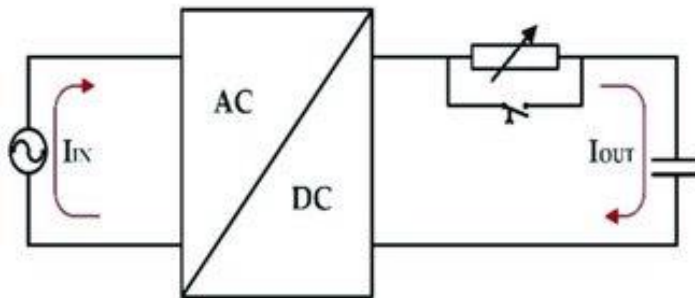
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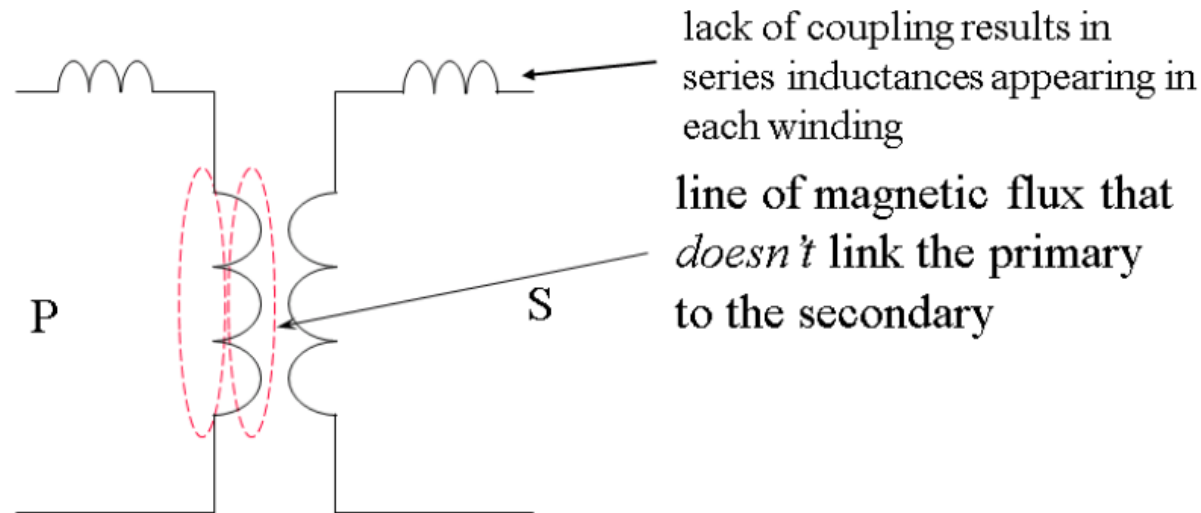
Design Requirements

- Leakage inductance:
 - For most of IC's application notes, they set a rule of thumb for leakage inductance of Flyback to be between **3-5%** of main inductance. **Does that make sense?**
- Because of that, let's understand the effect of leakage inductance in Flyback topology

FLYBACK TRANSFORMER

Design Requirements

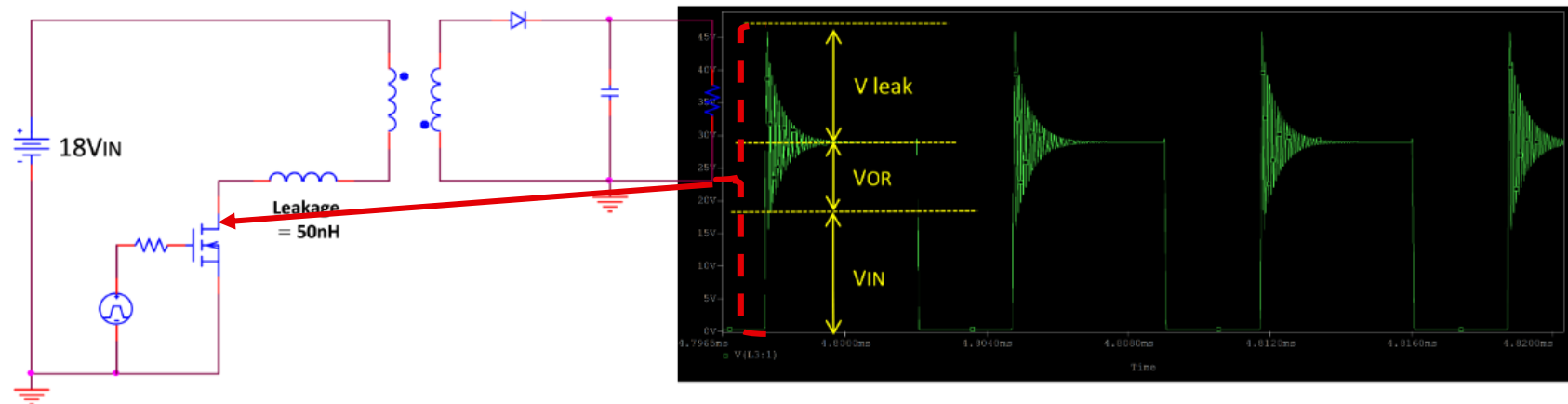
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FLYBACK TRANSFORMER

Design Requirements

- Leakage inductance:
 - Acts as discrete inductance in Flyback where during Switch ON, it can store energy (charge) similar to Prim inductance but when the Switch is OFF, leakage inductance discharge all energy on switch node casuses high spike votlage on switch node:



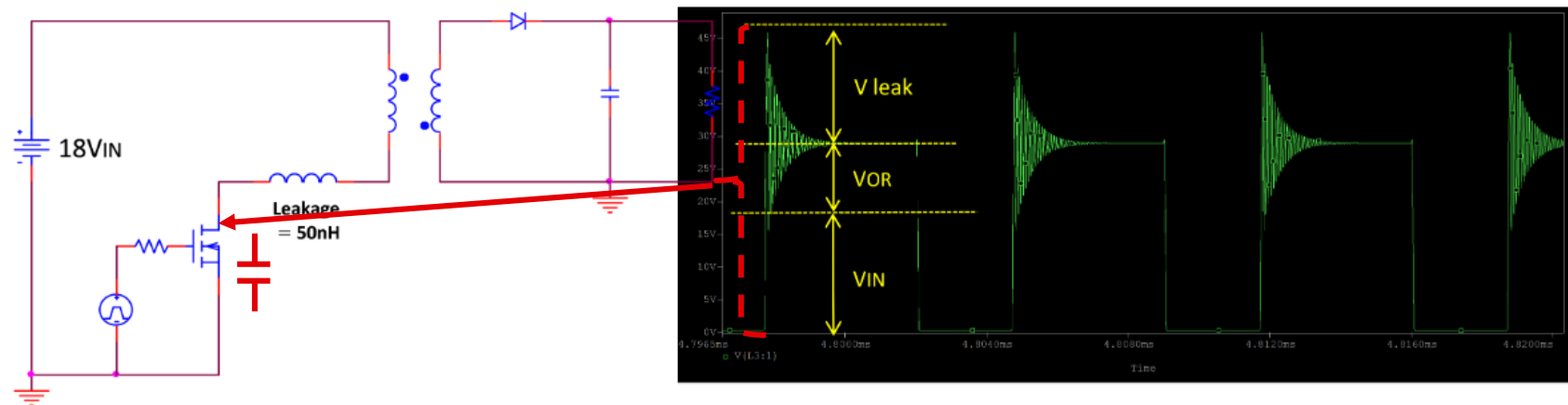
Switch Note Waveform with Leakage Inductance

Reference: Application note SLVAF01, Texas Instruments

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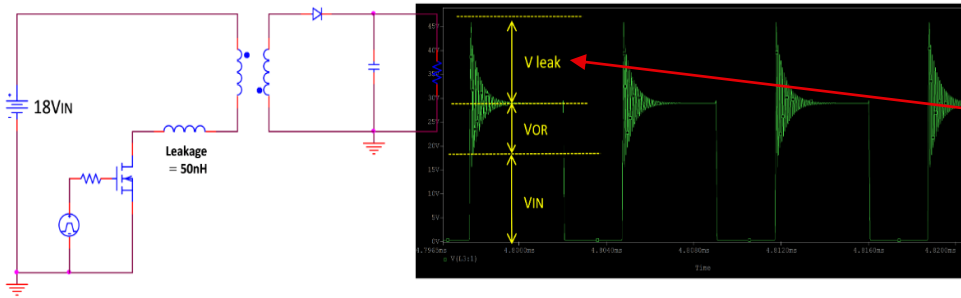
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FLYBACK TRANSFORMER

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Switch Note Waveform with Leakage Inductance

$$V_{leak\ or\ Spike} = I_{Pri-peak} \sqrt{\frac{L_{leakage}}{(C_p + C_{ds})}}$$

Where:

$L_{leakage}$: Primary leakage inductance

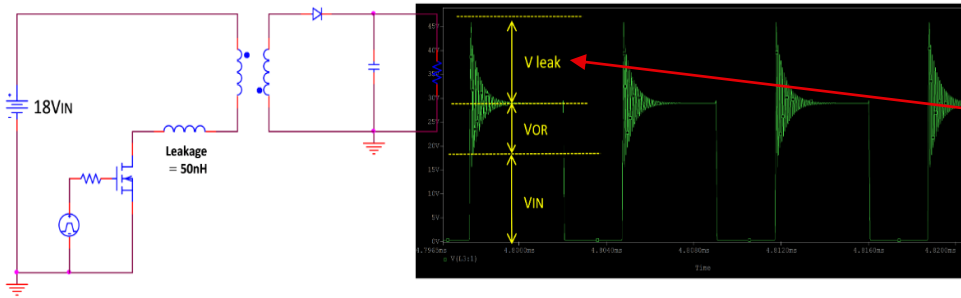
C_p : Transformer primary capacitance

C_{ds} : Mosfet drain-source capacitance

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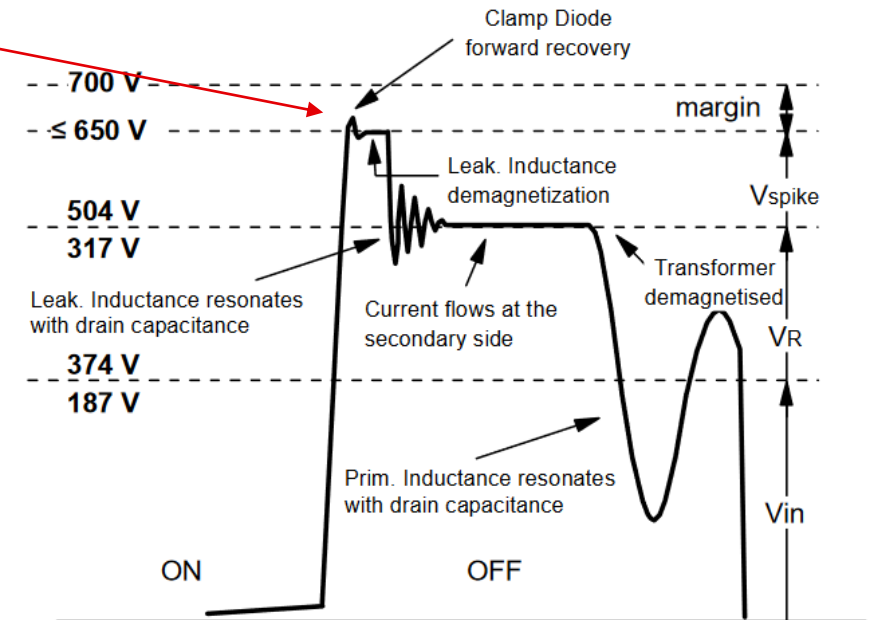
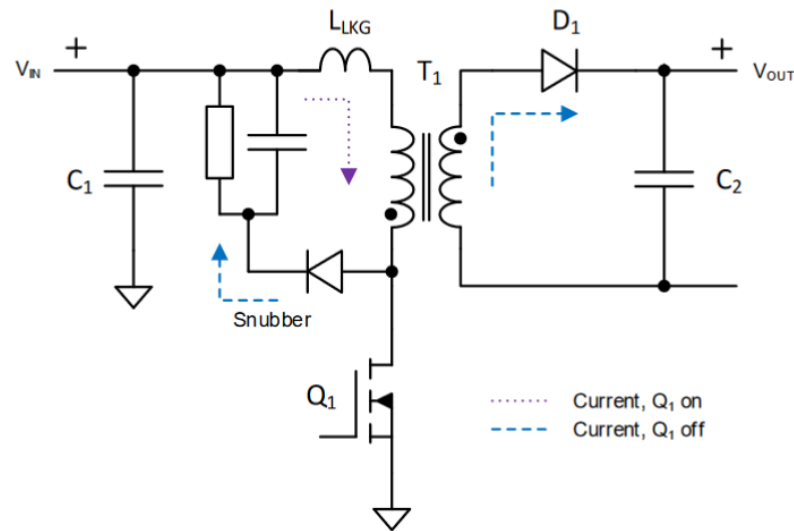
C_{ds} : Mosfet drain-source capacitance

$$V_{leak\ or\ spike} \propto I_{Pri-peak} \sqrt{\overset{\uparrow}{L_{leakage}} \over (C_p + C_{ds})}$$

FLYBACK TRANSFORMER

Design Requirements

- Leakage inductance:
 - On system level solutions:
 - Snubber circuit
 - Or Zener/TVS clamping
 - Mosfet with higher breakdown voltage
 -

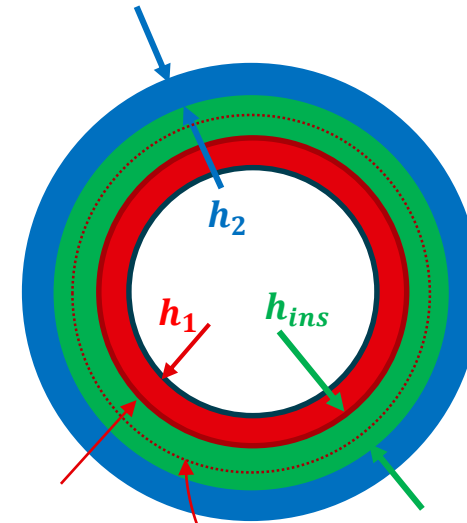
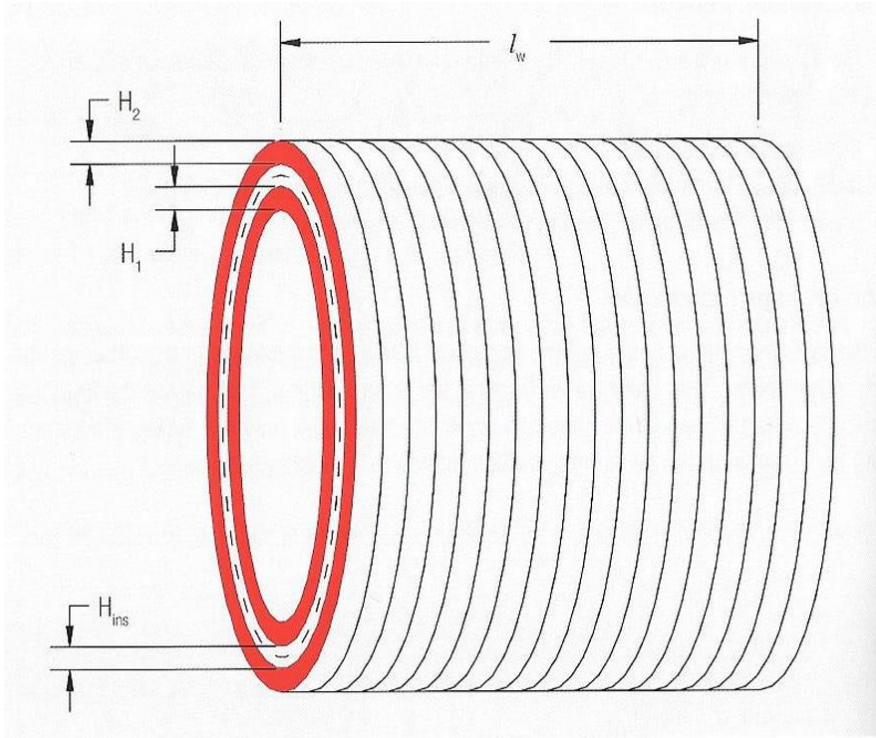


Reference: Application note AN1262, ST Micro

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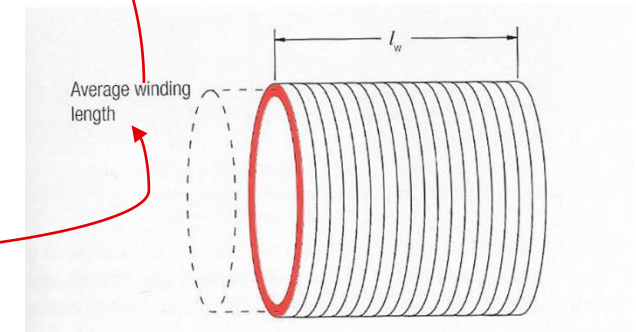
- Leakage inductance:
 - On component level:
 - **For Solenoid Structure with symmetrical turns ratio:**



$$L_{leakage} = \frac{\mu_0 N^2 A_{insulation}}{l_w}$$

$$A_{insulation} = \underbrace{MLT}_{\text{Average winding length}} \left(h_{ins} + \frac{1}{3} h_1 + \frac{1}{3} h_2 \right)$$

MLT: Mean length turn or average winding length

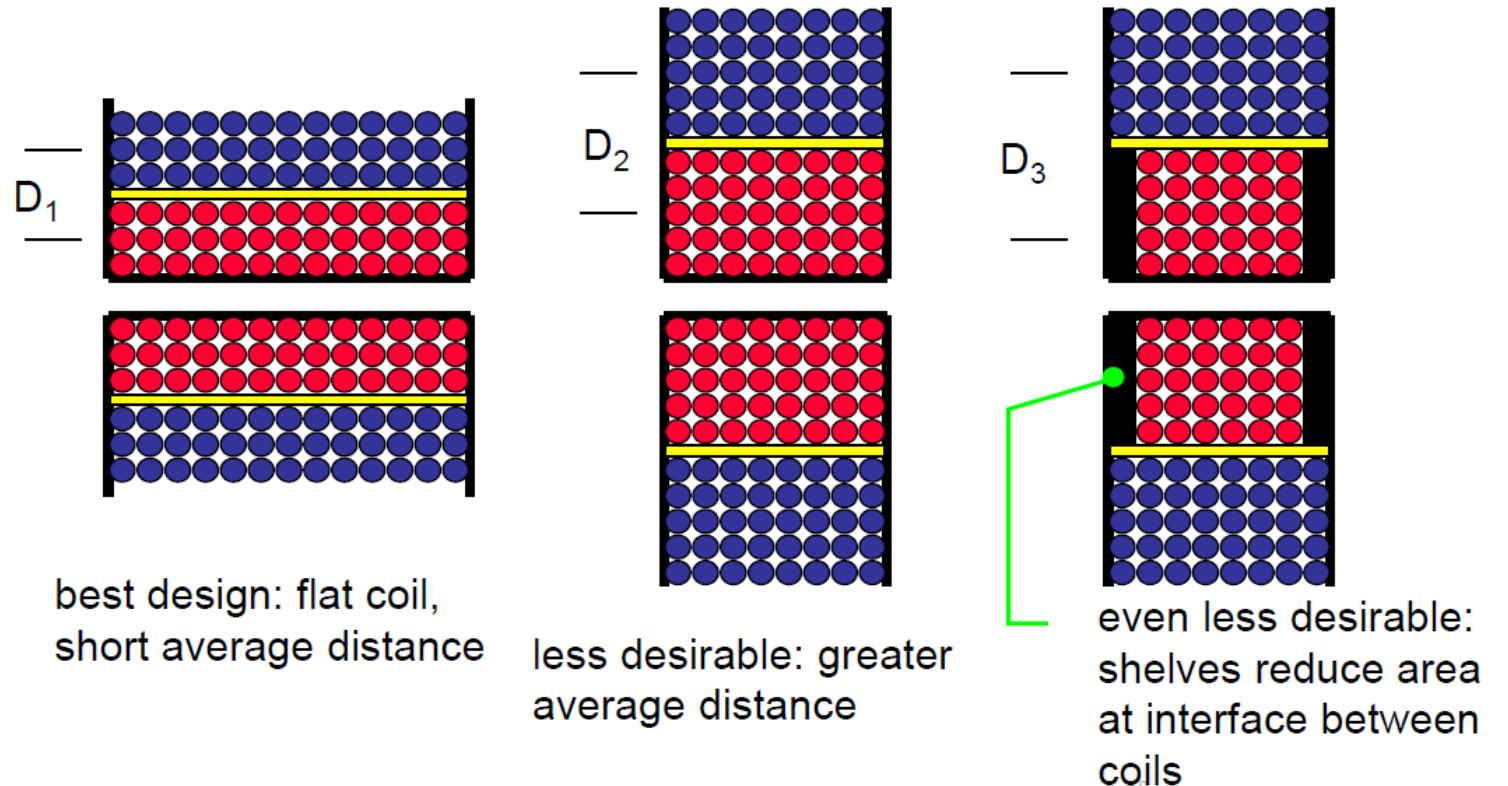


Reference: Würth Elektronik eiSos, Trilogy of Magnetics, handbook

FLYBACK TRANSFORMER

Design Requirements

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 - Examples**

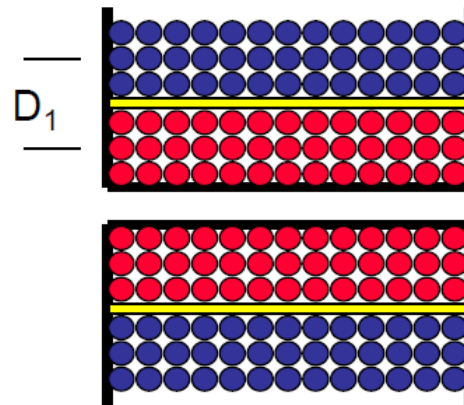


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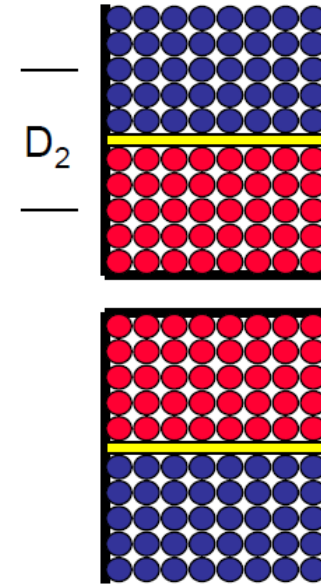
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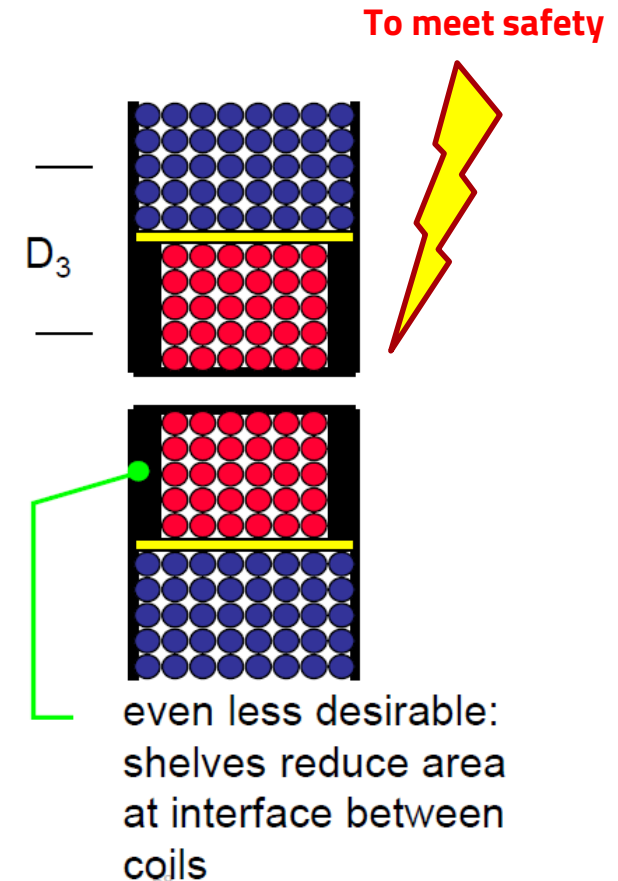
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best design: flat coil,
short average distance



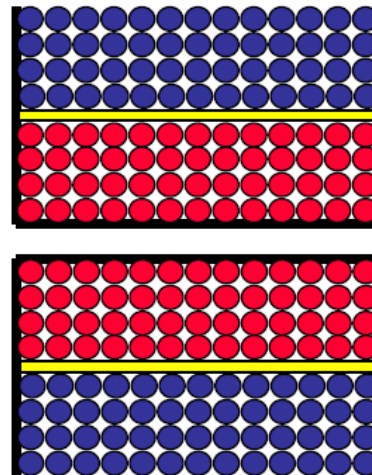
less desirable: greater
average distance



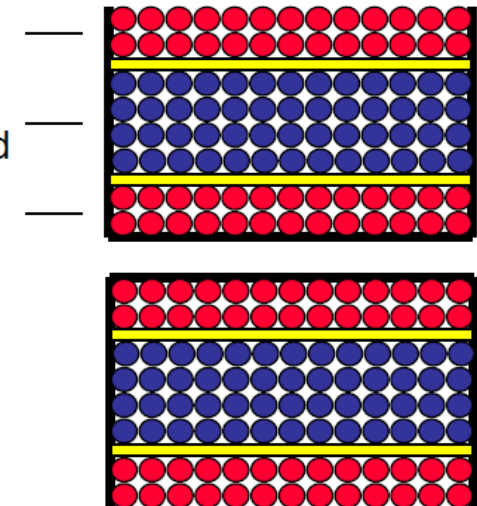
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The first winding is split around the second

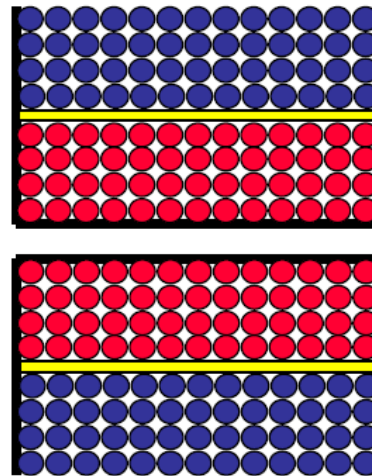


To improve the coupling between the windings we can **sandwich** the first winding around the second. This reduces the average distance between the windings and results in **1/4th** the original value of leakage inductance –

FLYBACK TRANSFORMER

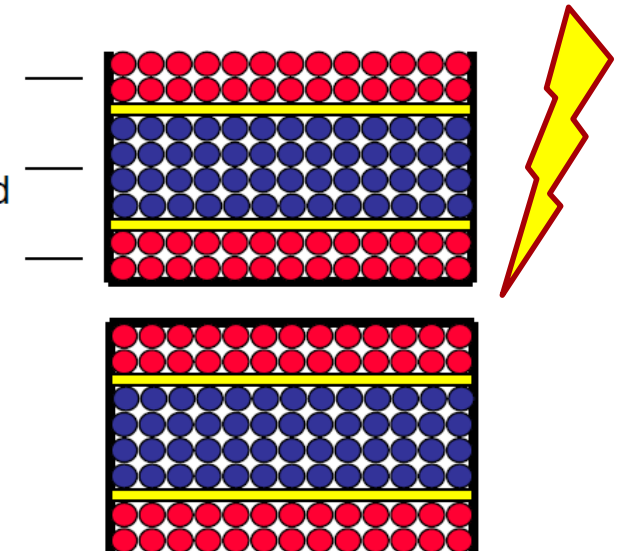
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The first winding is split around the second

More winding labor - \$\$ cost

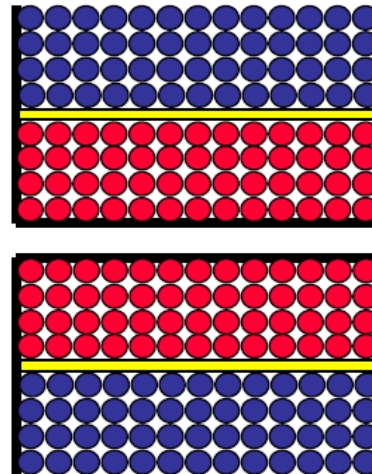
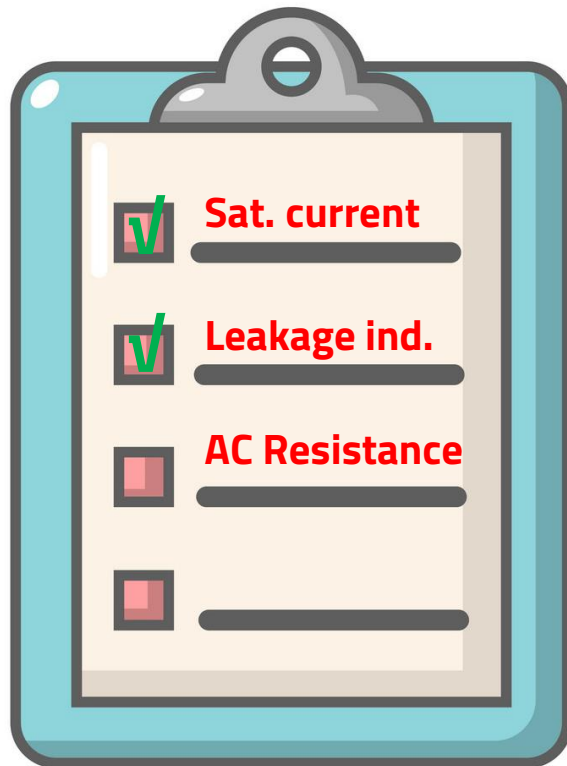


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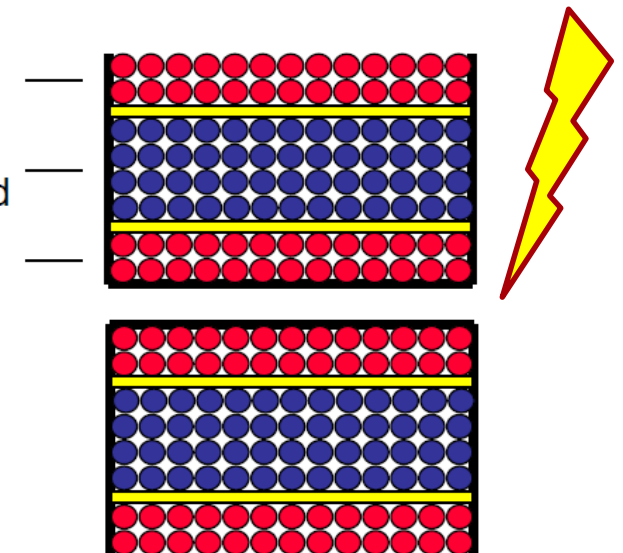
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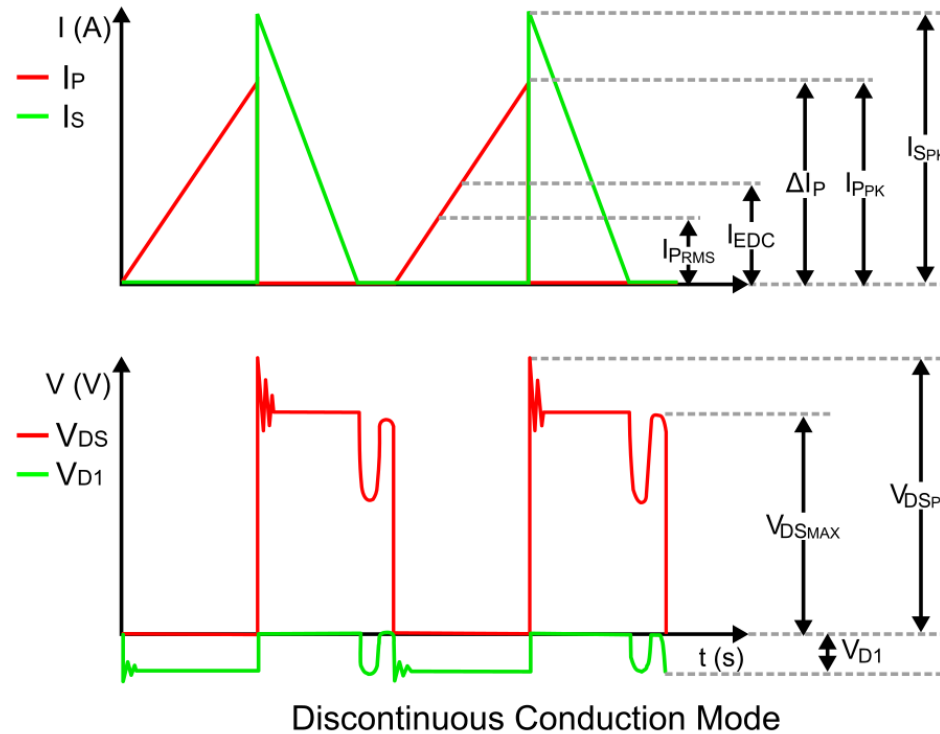


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FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Important of this resistance for DCM mode of operation.

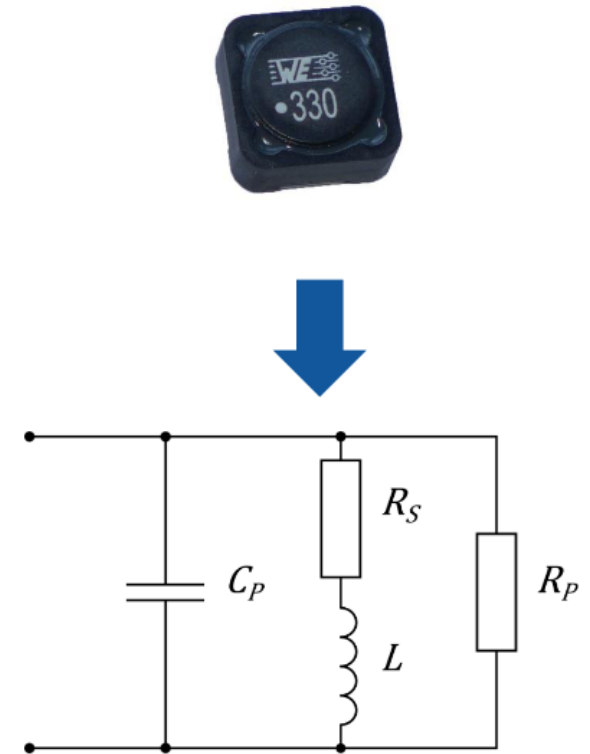
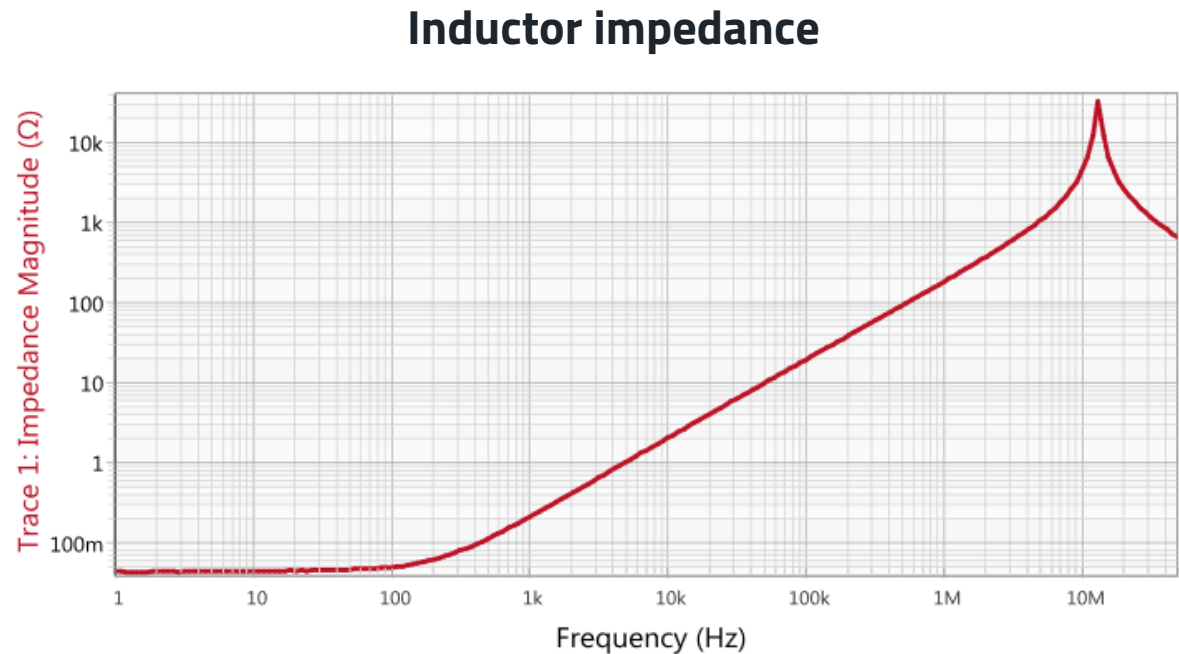


- Sawtooth current waveform on PRI & SEC**
- FFT of current waveform shows a fundamental @ switching frequency + harmonics**
- So importance of AC resistance comes to the equation**

FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Important of this resistance appears in DCM mode of operation or high ripple current mode.
 - At higher frequencies, AC resistance is the dominant for copper losses



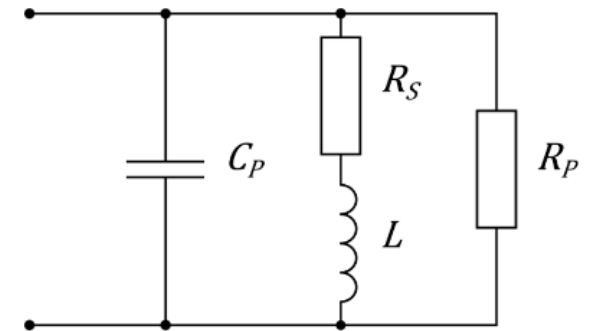
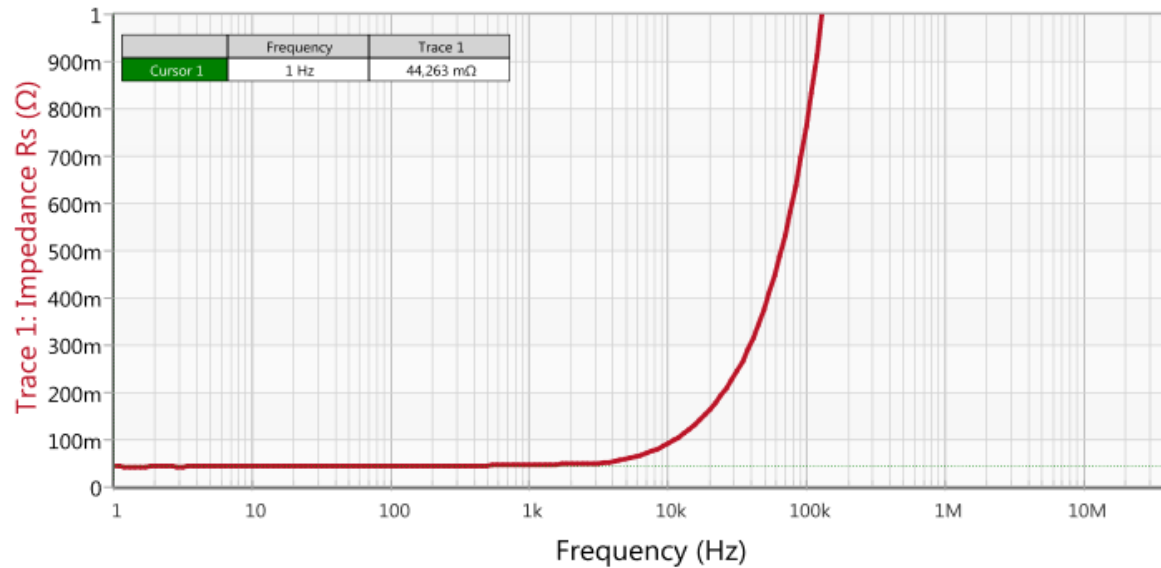
Reference: Bode 100 – Application note

FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Important of this resistance appears in DCM mode of operation or high ripple current mode.
 - At higher frequencies, AC resistance is the dominant for copper losses

R_s (AC component)



Reference: Bode 100 – Application note

FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Important of this resistance appears in DCM mode of operation.
 - At higher frequencies, AC resistance is the dominant for copper losses
 - Modeling of AC resistance:
 - Analytical or theoretical model -> **not easy (check text books)**
 - **Need to study the effect of:**
 - **Proximity effect**
 - **Skin depth**
 - **2D or 3D model using FEM:**
 - **Ansys -> Maxwell**

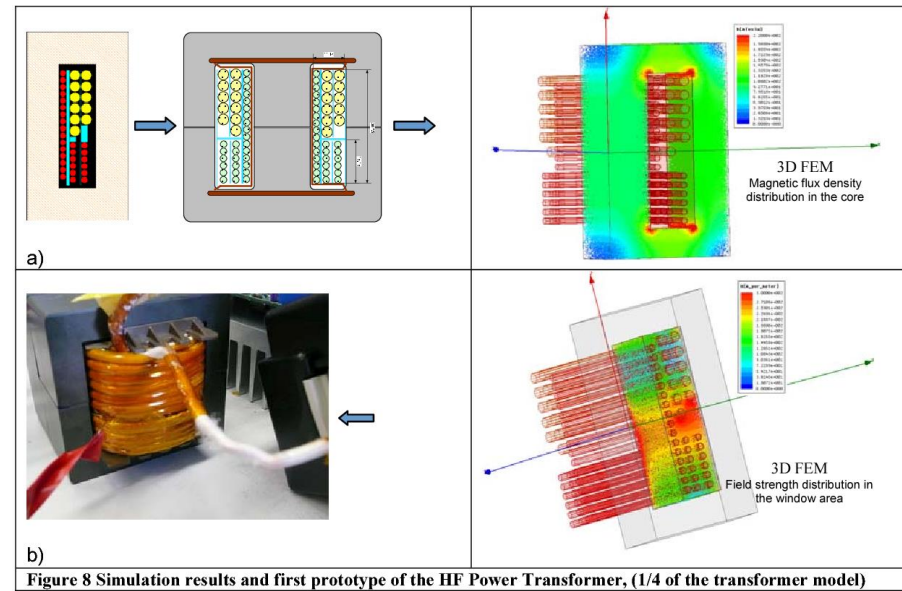
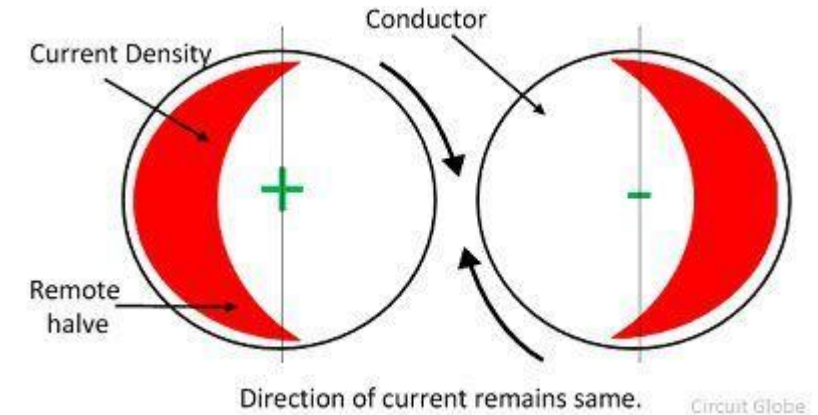
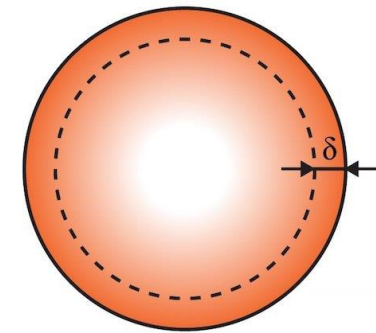


Figure 8 Simulation results and first prototype of the HF Power Transformer, (1/4 of the transformer model)



Skin Depth is:

$$\delta = \sqrt{\frac{1}{\pi f \mu_0 \mu_r \sigma_0 \sigma_r}}$$

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FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Litz wire to optimize AC resistance



FLYBACK TRANSFORMER

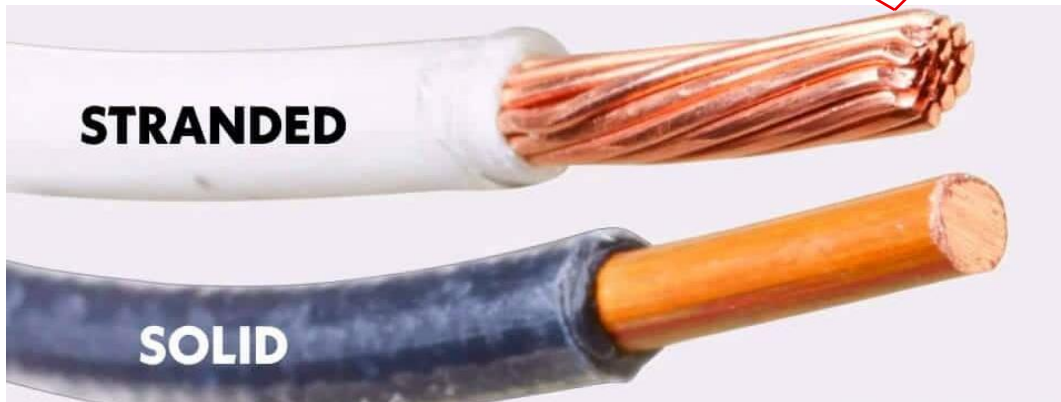
Design Requirements

- AC Resistance:
 - Litz wire to optimize AC resistance



Multi-strands wire

Twisted



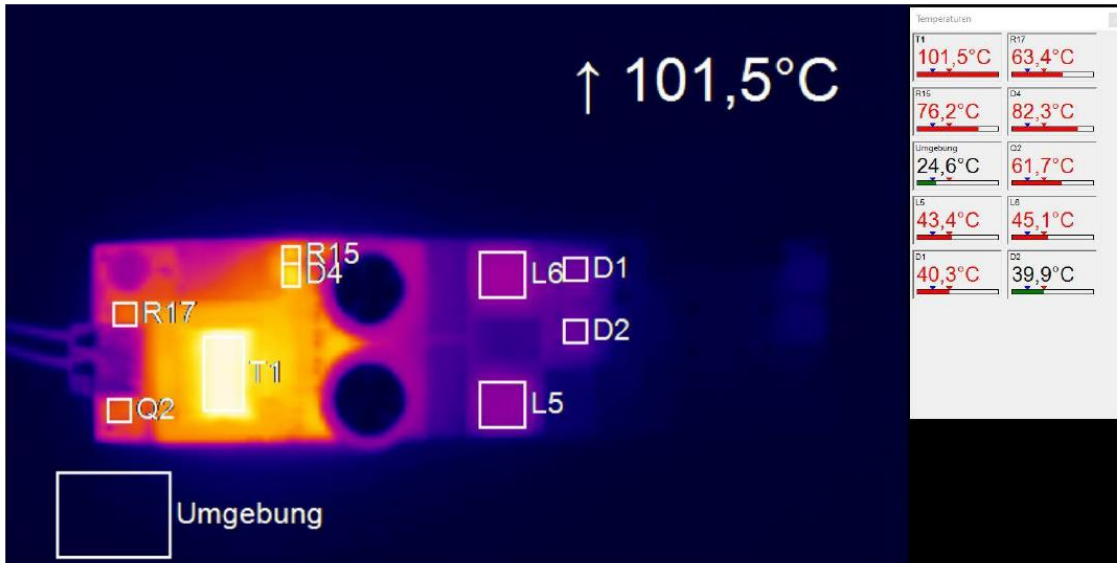
FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Litz wire to optimize AC resistance
 - Example:
 - Transformer for Offline flyback DCM topology at 100kHz operating freq.**



Line: 230V / Load: 30W

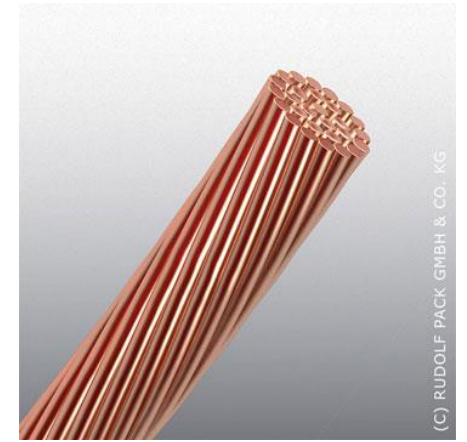


Transformer with solid wire

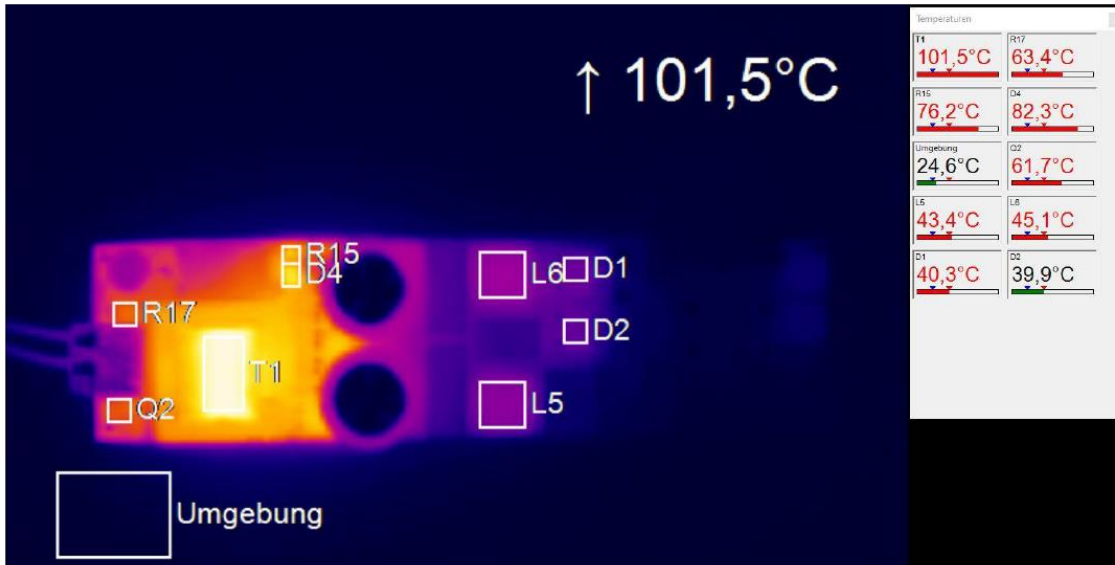
FLYBACK TRANSFORMER

Design Requirements

- AC Resistance:
 - Litz wire to optimize AC resistance
 - Example:
 - Transformer for Offline flyback DCM topology at 100kHz operating freq.**

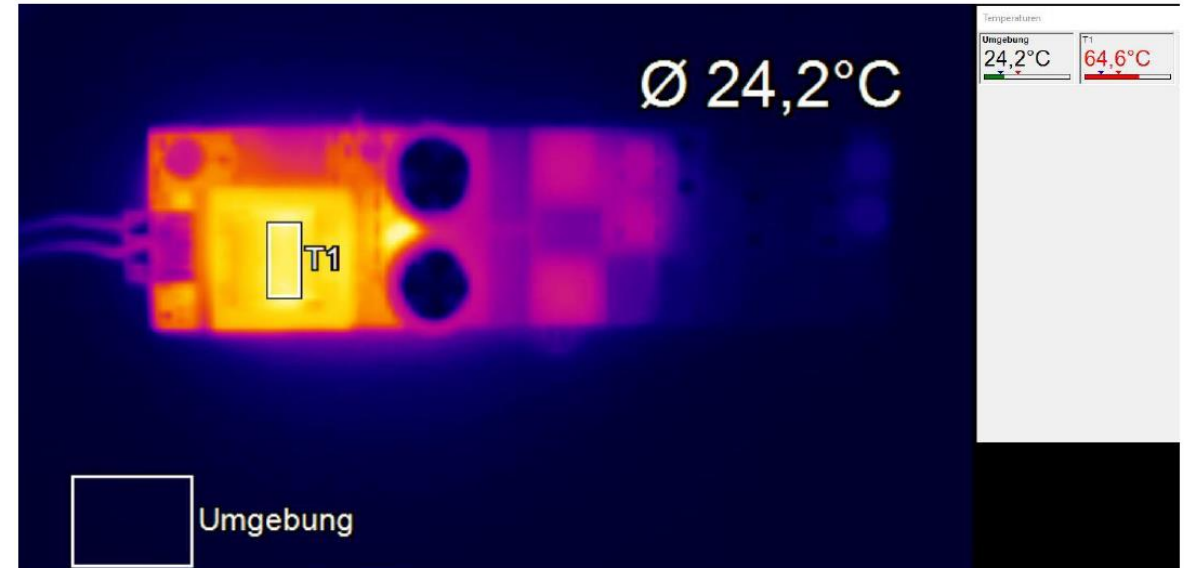


Line: 230V / Load: 30W



Transformer with solid wire

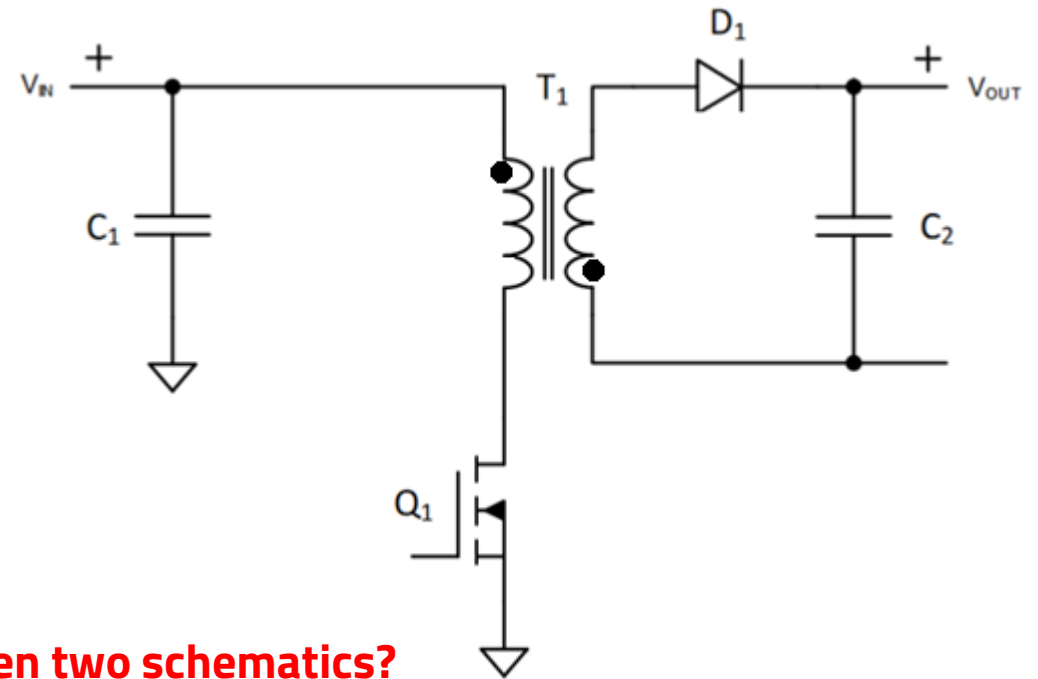
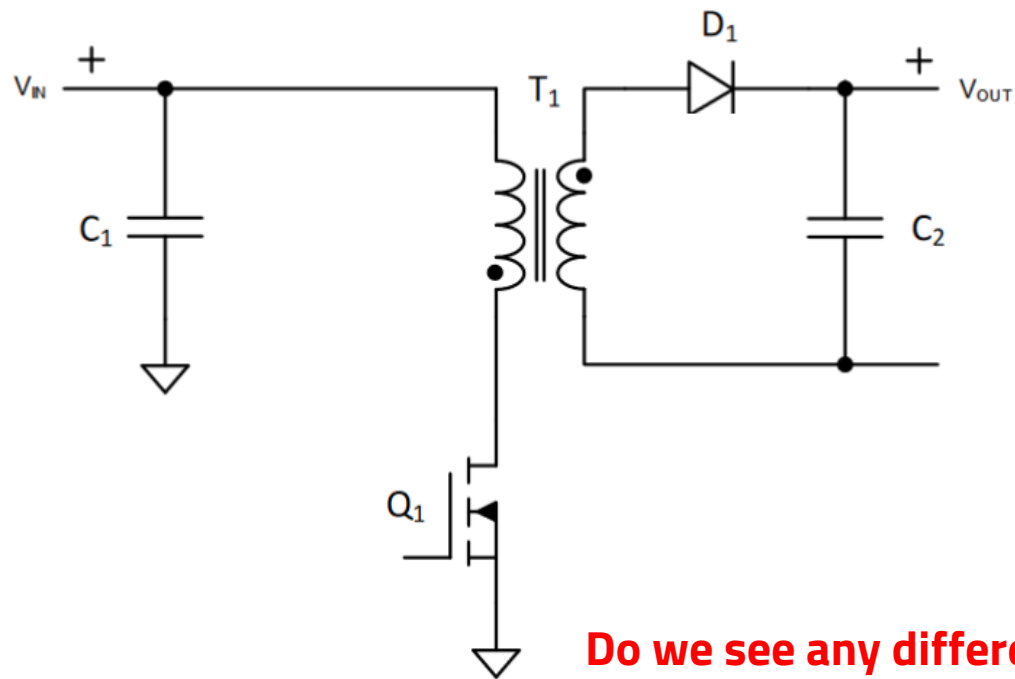
Line: 230V / Load: 30W



Optimized transformer using litz wire

TIPS TO IMPROVE EMI

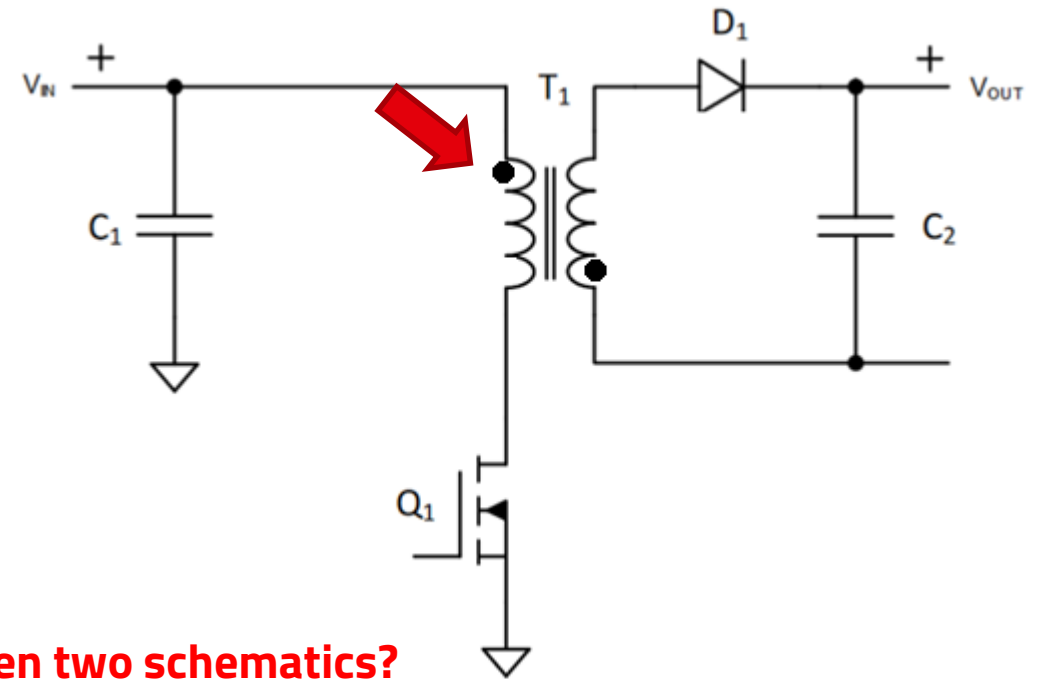
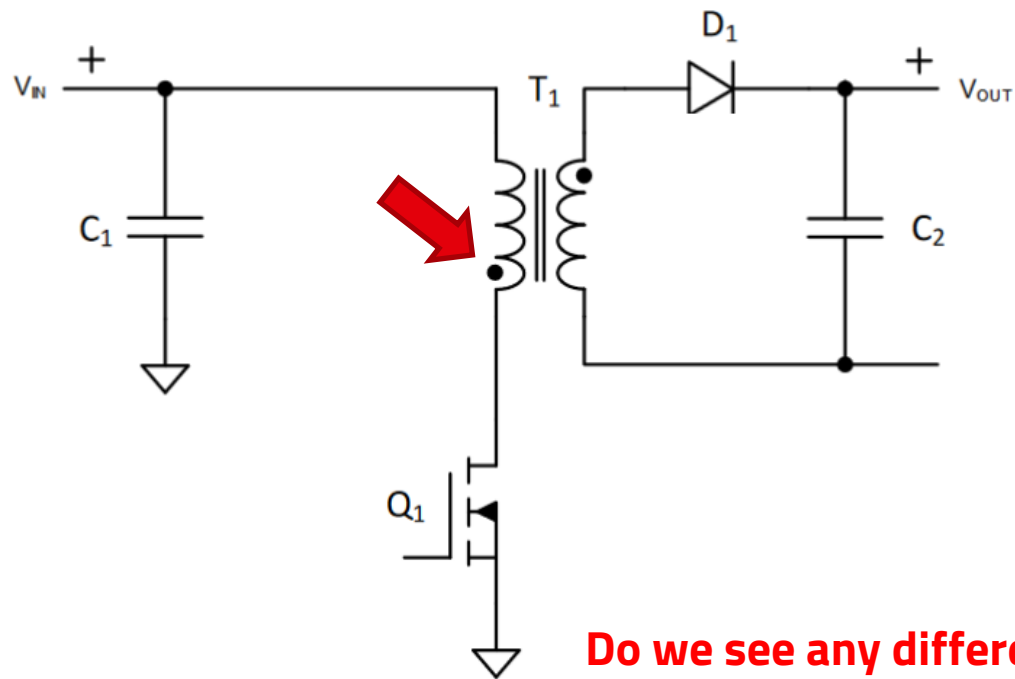
- EMI:



Do we see any difference between two schematics?

TIPS TO IMPROVE EMI

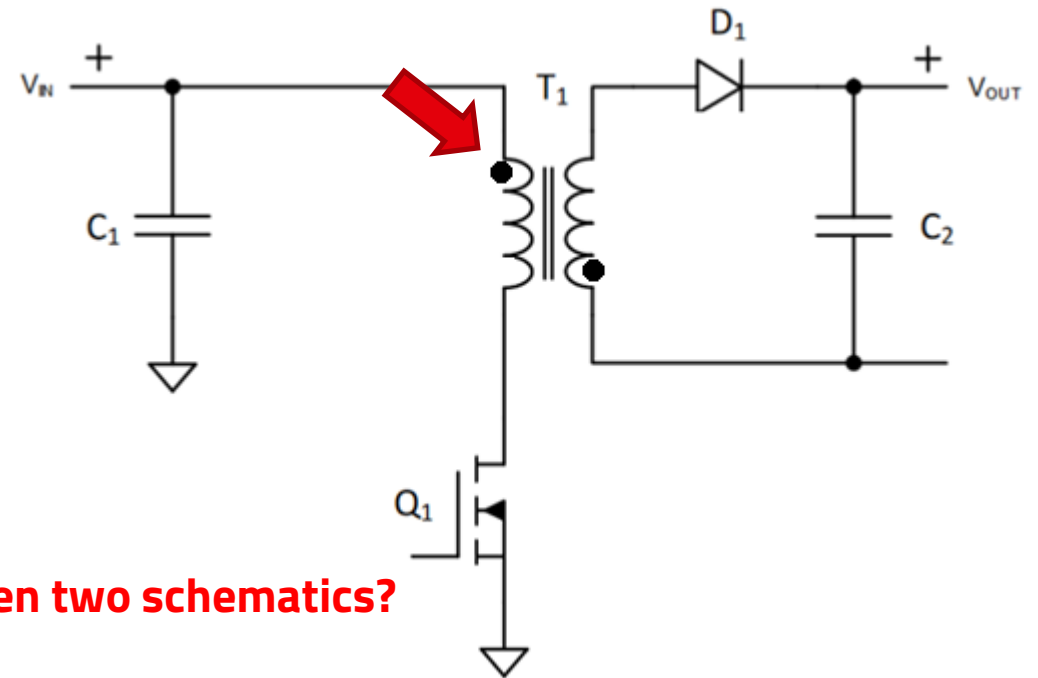
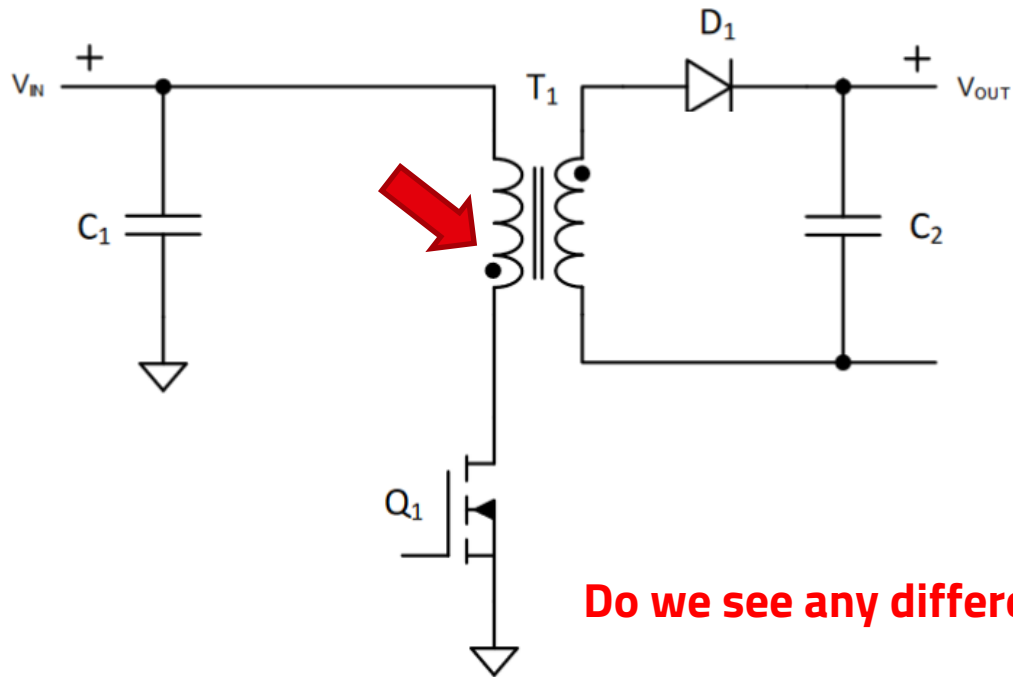
- EMI:



Do we see any difference between two schematics?

TIPS TO IMPROVE EMI

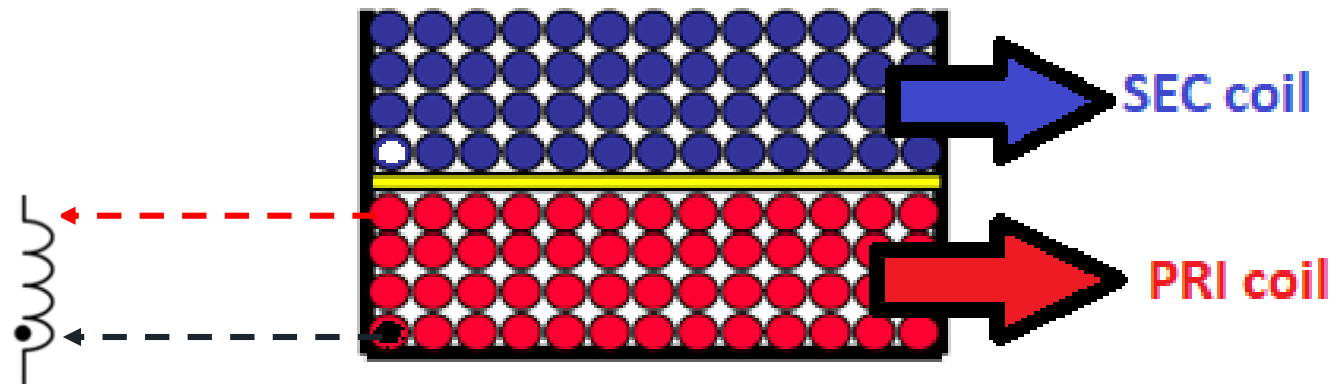
- EMI:
 - No difference on functionality of topology or circuit operation
 - But** it has impact on EMI performance



Do we see any difference between two schematics?

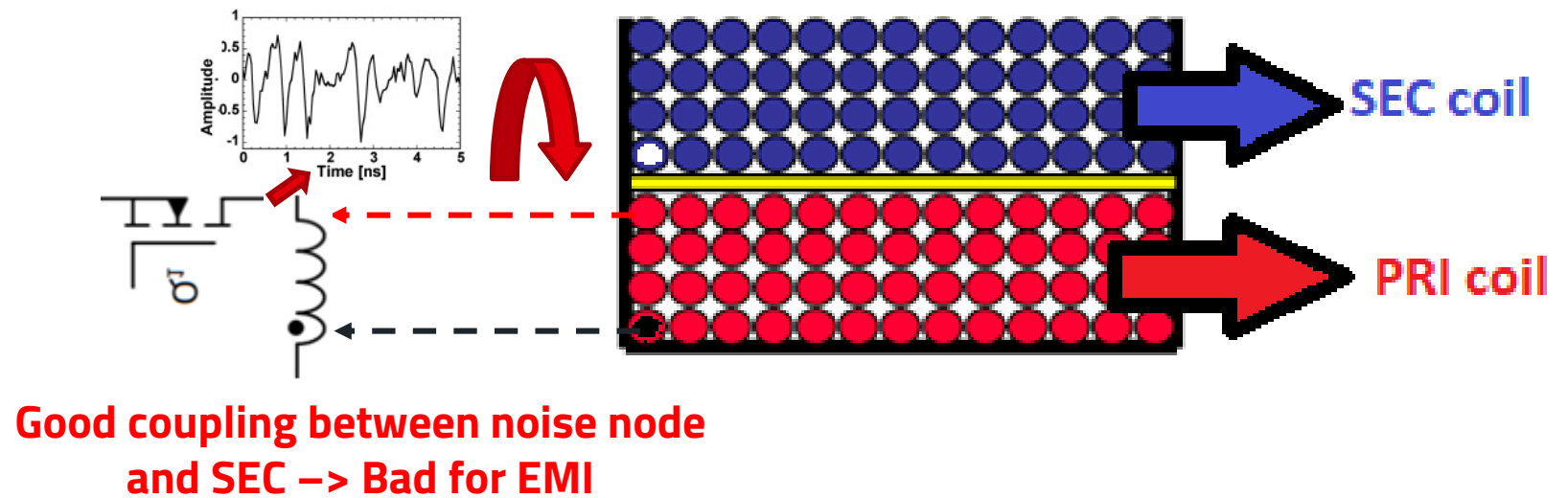
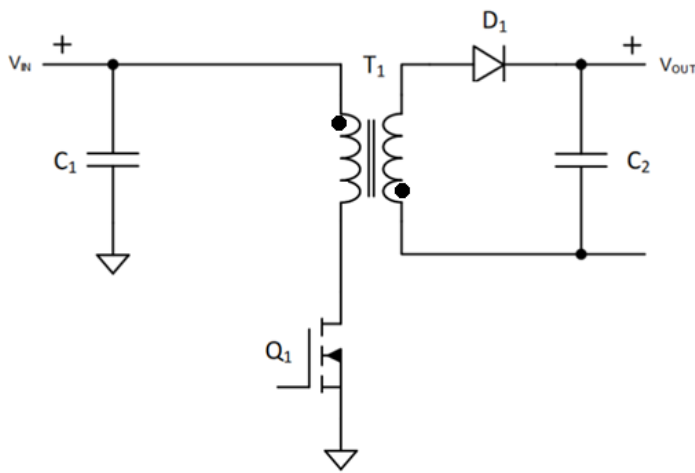
TIPS TO IMPROVE EMI

- EMI:
 - No difference on functionality of topology or circuit operation
 - **But** it has impact on EMI performance



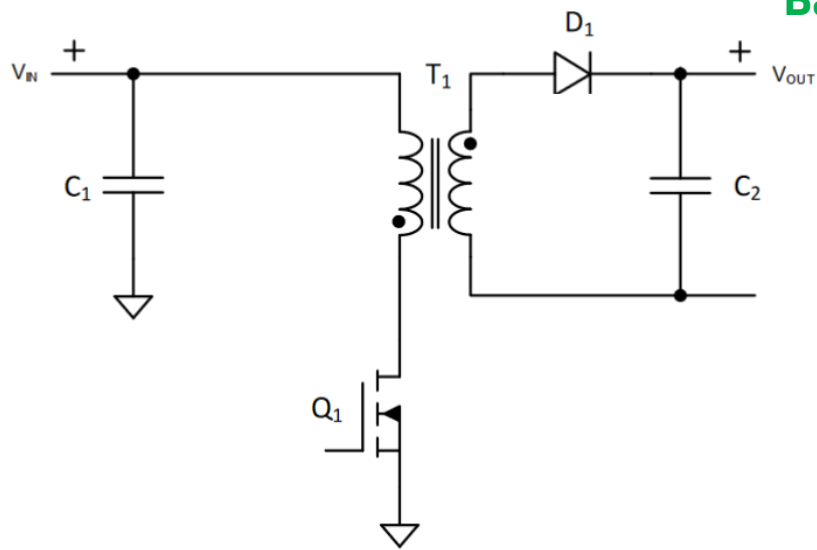
TIPS TO IMPROVE EMI

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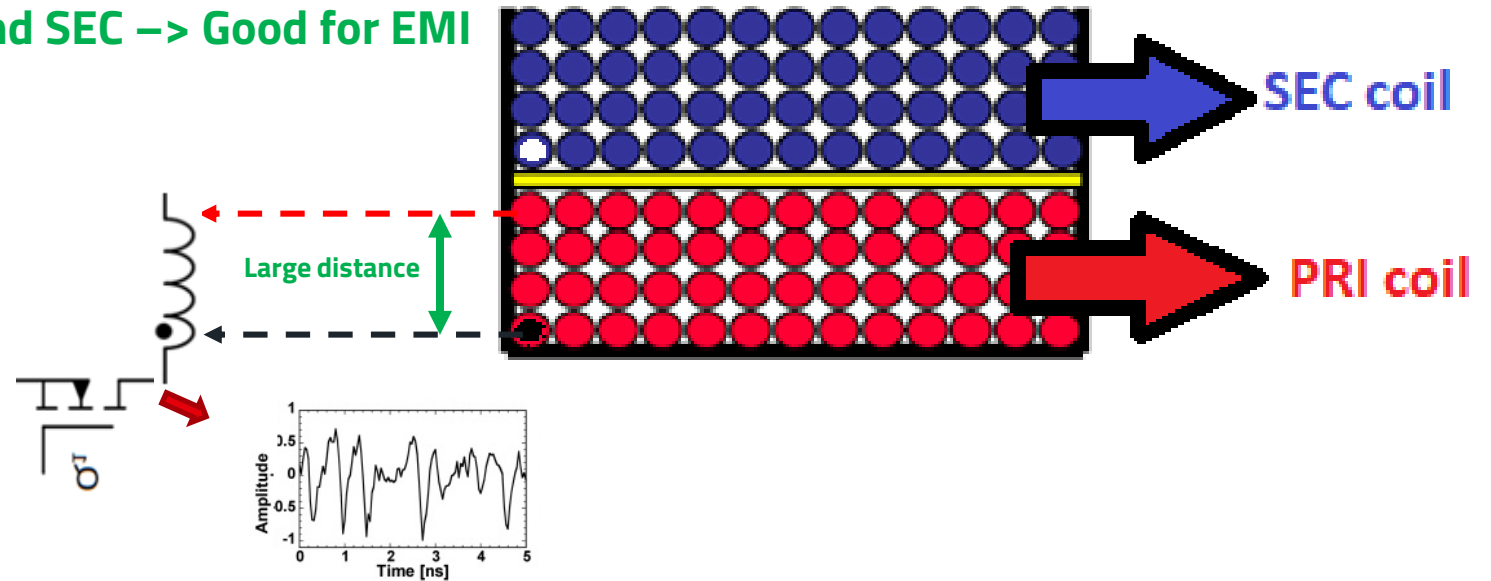


TIPS TO IMPROVE EMI

- EMI:
 - No difference on functionality of topology or circuit operation
 - But** it has impact on EMI performance



Bad coupling between noise node
and SEC → Good for EMI



TIPS TO IMPROVE EMI

- EMI:
 - Würth Elektronik article for Buck inductor:
 - EM Radiation due to the Influence of the Start of the Winding in an Inductor

https://www.we-online.com/web/en/electronic_components/news_pbs/blog_pbcm/blog_detail-worldofelectronics_109450.php

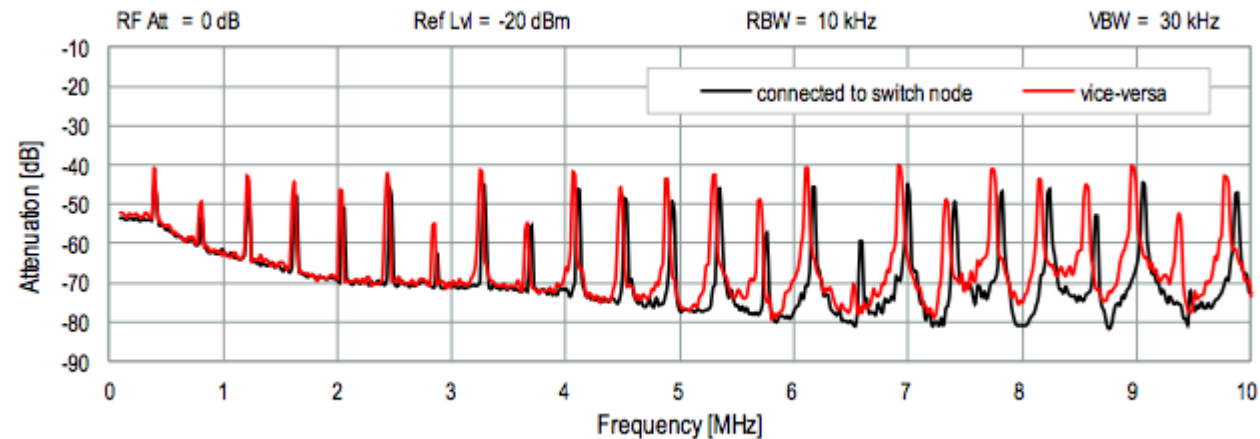


Figure 7: E-field of the inductor's start of winding connected to the switch node and vice-versa

Questions

& Answers



We are here for you now!
Ask us directly via our chat or via E-Mail.

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Khaled.Elshafey@we-online.de